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OCEANOGRAPHIC INVESTIGATION OF THE MARGINAL SEA ICE ZONE OF THE CHUKCHI SEA-- MIZPAC 1974

Ъу

R. G. Paquette and R. H. Bourke

A report submitted to Director, Arctic Submarine Laboratory Naval Undersea Center, San Diego

May 1976

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20. ABSTRACT (Continue on reverse side if necessary and identify by block number)

Continuous profiles of temperature and salinity (STD observations) were made in the shallow (~45 m) Bering and Chukchi Seas in July 1974 as part of the MIZPAC program. In addition to measurements in ice-free waters, seven closely spaced crossings of the sea-ice margin were made along with two crossings of the Alaskan coastal zone. In all, 111 STD stations and approximately 100 XBT drops were made for which graphs and tabulations were produced of temperature, salinity, density and sound speed.

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South of the ice the water is sharply layered with a warm fresh layer $(8\text{-}10^{\circ}\text{ C} \text{ and } \sim 10\text{m} \text{ thick})$ above a cold dense layer. At or near the sea-ice margin the layering gradually disappears with modification of isopycnals and isotherms extending to the bottom. Large scale temperature fluctuations of 0.5 to 2° C, termed mesostructure, were observed at 12-15m depth in the first three crossings, but were weak or absent in the other crossings. Mesostructure appears to be correlated with a relatively rapid melting of the ice, and hence, probably with a strong northward flow, or a diffuse ice margin. Mesostructure formation is believed to result from non-uniform lateral mixing of waters of different temperatures but the same density, possibly modified or controlled by a complex lateral pressure field near the ice.

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I. INTRODUCTION

This report describes the results of a cruise, termed MIZPAC 74, conducted in the northern Bering Sea and in the sea-ice margin of the Chukchi Sea to examine the processes which lead to mesoscale temperature structure in the water column. The field work was carried out from the icebreaker USCGC BURTON ISLAND during the period 13-30 July 1974 using a continuously profiling instrument.

These oceanographic investigations of the marginal sea-ice zone are part of a long-term program, Project MIZPAC, which is under the direction of the Arctic Submarine Laboratory, Naval Undersea Center, San Diego. Applied objectives of MIZPAC include development of arctic submarine technology and enhanced understanding of the complex acoustic environment of the MIZ. Personnel from the Applied Physics Laboratory, University of Washington (APL) also participated in MIZPAC 74 taking acoustic and biological and physical measurements. Their temperature and salinity data were taken concurrent with our observations using a different instrument, the conductivity-temperature-depth recorder (CTD) built by APL.

This cruise was the third in a series of cruises conducted in the Pacific marginal sea-ice zone (MIZ) in which personnel from the Naval Postgraduate School have participated. Previous cruises in July and August of 1971 and 1972 in the Chukchi and Beaufort Seas have established the presence of a thermal mesostructure near the ice edge which appears to be highly variable over short time and space scales (Paquette and Bourke, 1973). The primary purpose of this cruise was to obtain many closely spaced samples of the thermal structure over a large area of the MIZ to further establish the character of the

mesostructure, its distribution and strength relative to its distance from the ice edge, and the probable oceanographic mechanisms which cause it to form.

II. GENERAL PROCEDURE

A. TECHNIQUES

As in the previous two cruises in 1971 and 1972, the primary instrument was the Bissett-Berman Model 9006 STD kindly loaned by the Arctic Submarine Laboratory. This is an "Arctic" model because of the extended temperature scale to -2°C . However, the instrument has to be modified with the application of a 400 ohm resistive shunt to read salinities lower than 30 $^{\circ}/_{00}$, its nominal lower limit. Two lowerings of the STD were therefore required for stations located in the immediate vicinity of the ice; the upper portion of the water column was recorded with the shunt, the remainder without the shunt. The effect of the shunt and the errors introduced due to the lag in the compensating thermometer of the salinity sensor are described in the report summarizing the MIZPAC 71 and 72 cruises (Paquette and Bourke, 1973). The manner of correcting these errors is described in Part C of this section.

The STD was standardized at most of the stations by means of a Nansen bottle, just above the instrument, which was tripped at the maximum depth of lowering. The salinity and temperature offsets were found to be reasonably constant over long periods; during these periods constant additive corrections were applied throughout the water column. The standard deviations in the temperature and salinity errors approximated 0.04° C and 0.02 o/oo, respectively.

Bucket samples of salinity and temperature were taken at most of the stations. They could not be used for standardization because of the large gradients between the surface skin and the approximate one meter depth of the STD. The bucket measurements were incorporated in the final digital data at zero depth. Later, it was found that the detail in the upper meter of water had a considerable effect on the dynamic heights. Data from the CTD measurements of APL were used to supply this detail where necessary.

Shallow-water XBT's (Model T-10) were used to supplement the STD measurements. The XBT recorder was modified by replacing the chart-drive motor by a faster motor and using a chart paper calibrated for 200 m maximum depth. This has the effect of expanding the depth axis of the temperature trace. Mesostructure could be observed but the XBT has too rapid a rate of fall or, conversely, too slow a temperature sensor to reproduce the mesostructure faithfully and the features are therefore somewhat smoothed.

The general observational technique was to make closely spaced measurements on a line normal to the ice edge starting 10 n mi outside and penetrating 10 n mi into the ice or to a distance where the structure vanished. Penetrations were usually 30 n mi apart.

B. CRUISE PLAN

Figure 1 is a map showing the positions of the one hundred and eleven stations occupied during MIZPAC 74. Equipment problems with the STD eliminated observations at Stations 1,3,4, 12, 13, and 41, but data from the APL's CTD are available for these stations. Data taken during the early part of the cruise (while transiting to the ice margin) were

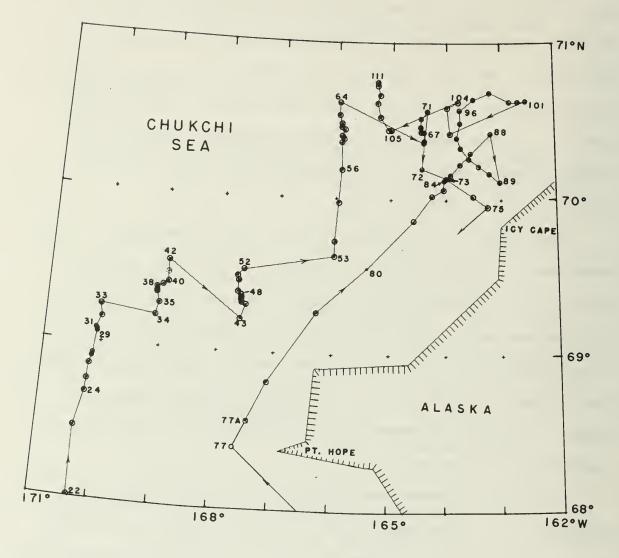


Figure 1. MIZPAC 74 STD station positions.

for the purpose of establishing the characteristics of the water flowing into the Chukchi Sea. A little ice was first encountered at Station 27; a better defined ice margin was at Station 29. The ice margin was initially quite diffuse and some trouble was experienced in locating and defining the ice edge. There was no good distant overview to tell when the ice seen dimly ahead through the fog or on radar was a substantial margin or only a line of large floes. Therefore, the ice margin is sometimes poorly defined, and some crossings contain the complicating influence of isolated patches of diffuse ice well south of a denser margin. On 24 July, midway into the cruise, strong winds from the south developed, causing the ice margin to become compact and characterized thereafter by 8 oktas of ice.

Seven ice-margin crossings were made during the cruise. These were the station sequences 24-33, 34-42, 43-52, 53-64, 65-71, 93-98, and 105-111. For convenience these are called Crossings Nos. 1 to 7, respectively. In addition, two crossings of the warm coastal current and a transect along its axis were made. Nine XBT transects of 7-10 observations each were made, most of them while retreating from points of maximum ice penetration (Figure 2). It was expected that this procedure would give a more nearly synoptic picture of the temperatures in the cross-section and that there might be some advantage in accuracy and uniformity of spacing compared with the time-consuming STD stations during which the ship could drift.

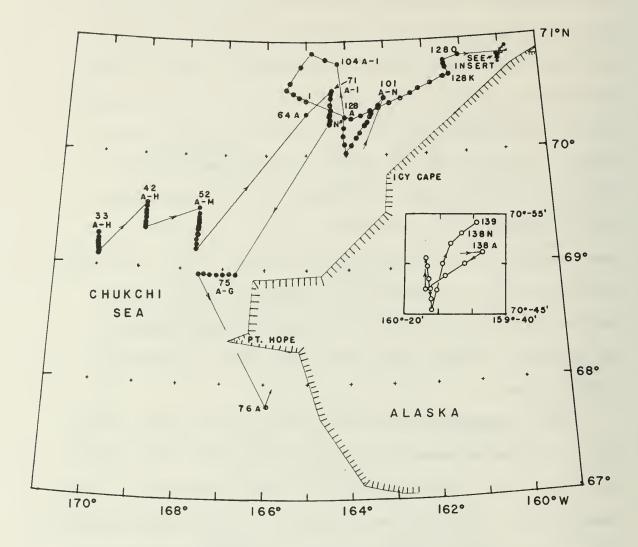


Figure 2. MIZPAC 74 XBT station positions.

C. REDUCTION OF DATA

The same data reduction techniques as employed previously (Paquette and Bourke, 1973) were used on the 1974 data with some minor changes. Basically the procedure was to trace the original STD plots with the Calma digitizer and to use a computer program, MIZ2, which converts the digitizer tapes to corrected temperatures and salinities, computes sound speed and sigma—t, and does a certain amount of editing prior to producing printed and tape outputs. Plots were then made of property profiles of each station.

For the 1974 data we initially attempted to treat the spiking which routinely appears in the temperature and salinity traces in a different fashion than previously. In the past we had faithfully traced the temperature profile, but eliminated any spikes while tracing the salinity curves. This time we first tried including all the temperature and salinity spikes during our tracing operations and attempted to remove the anomalous spiking with a first order response equation. This procedure was only partially successful presumably due to the large proportion of second and higher-order response in the thermal compensator. We then resorted to handsmoothing the salinity curves prior to tracing, being guided by the regions of the temperature curve where its slope was near zero and the salinity could be presumed to be undistorted. technique eliminates the possibility of finding salinity inversions and density inversions, but we believe the inversions which might exist are slight.

The plotting routines were modified to simplify data preparation and to obtain a more compact presentation. Property profiles from each STD station were plotted, four per page. These profiles along with the heading data for each station are in Appendixes I and II of this report. Both the shallow and deep lowerings are on the same plot. Occasionally, the overlap between the two lowerings is not perfect, causing a break to appear in the curves. The temperature trace is marked with crosses, and the salinity with dots every 20 depth increments, and we have occasionally introduced a small symbol (T, S, V, Σ) to help distinguish curves. The surface bucket measurements are marked on the abscissa by symbols, as above, but the curves are not drawn to them because of the resulting deterioration in legibility; property gradients in the top meter often are large.

Nested temperature profiles for each XBT line are shown in Appendix III along with the station heading data. The temperature traces are normally spaced 1° C apart with the deepest temperature printed below each trace. Occasionally, to avoid confusion with overlapping traces, the temperature offset was increased by an integral number of degrees. The tick marks on the abscissa are 1° C apart.

Vertical temperature profiles and temperature and sigma-t cross-sections were constructed for each of the seven ice-margin crossings. These are shown in Appendix IV.

III. RESULTS

A. GENERAL OCEANOGRAPHY

The waters south of Bering Strait, as one might expect, were fairly warm at the surface, 6° - 8° C, and sharply stratified, the upper layer extending to a depth of 10 - 20 m. However, the upper

layer had a salinity of about 32 o/oo, a fairly high value in view of the presumed northerly transport of water from the Yukon and Kuskokwim rivers. The lower layer was relatively cold, ranging between about 0° and 3° C, with salinity between 32 and 33 o/oo, only a few tenths of a unit more saline than the upper layer.

In Bering Strait warm surface water is present as a thin layer of about 5 m thickness along the eastern side. Stations 13 and 14 show surface temperatures of $8-10^{\circ}$ C, while 5 n mi farther westward surface temperatures are about 3° C. Below the warm layer, only at Station 13, and presumably eastward, is the water column fairly warm, remaining above 5.9° C at all depths. In the western portion of Bering Strait, Stations 14-16, temperatures are about $1-2^{\circ}$ C. With the exception of the shallow surface layer, the water column across Bering Strait is nearly isohaline and isopycnal. This is similar to the results shown by the Naval Oceanographic Office (1958) or NORTHWIND 1967 (Husby, 1969).

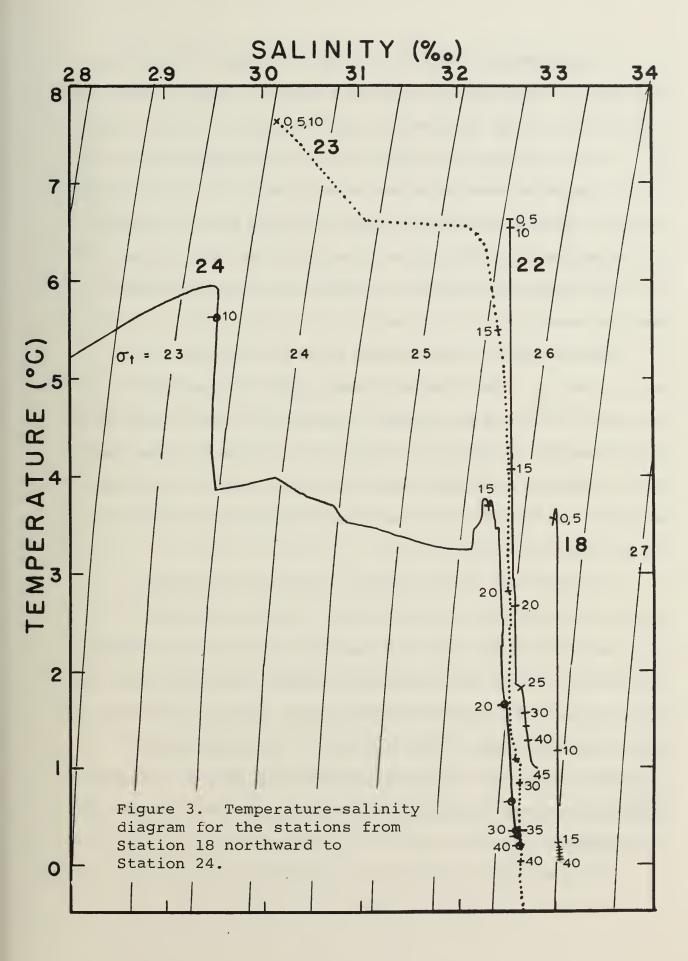
North of Bering Strait the water became more stratified again, at first only in temperature, at Station 22, but at Station 23 a pronounced decrease in salinity developed in the upper layer and was maintained farther north. The temperature of the upper layer rose toward the north, reaching a maximum of nearly 8°C at Station 23. At the next station, 18 nmi south of the then existing ice margin, the influence of the ice began to be noticeable. Not only was there pronounced surficial cooling, leaving a subsurface temperature maximum, but mesostructure began to develop and assumed various forms as the ship progressed through the ice margin at Station 29 and beyond. These relationships from Station 24 northward may be seen in Figure 7, and

the development of the upper stratum farther south in the temperaturesalinity diagram, Figure 3.

The development of a two-layered system between Station 22 and the ice is an interesting phenomenon. The sharply stratified upper layer at Station 23 cannot be presumed to originate in Bering Strait even if the waters there were less saline at an earlier date because the mixing which goes on there makes a thick, low-salinity upper stratum unlikely. The diminished salinity in the upper stratum can only have come from the melting of ice which was present north of Bering Strait. The resulting diluted layer must then have been pushed northward by the northward-flowing waters.

It is easy to demonstrate that the dilution is of the proper magnitude to correspond to the thickness of the ice cover. If one assumes an ice thickness of 140 cm, an ice salinity of 4 o/oo, and an ice density of 0.92, and computes the dilution of 12 m of a water column similar to Station 22 by the ice standing above it, the resulting salinity is 29.9 o/oo, very near the 30.2 o/oo observed for the upper layer of Station 23. Thus, the diminution in salinity is almost exactly as great as would correspond to the melting of a typical ice layer.

The position of this low-salinity layer at a distance of 147 n mi north of Bering Strait thus suggests a mean flow northward in the surface layers of 147 n mi during the forty days between 7 June, the the approximate date at which the ice margin passed Bering Strait, and 17 July. This corresponds to a mean velocity of 3.7 n mi/day or 0.15 knot.



A more meaningful result is in terms of transport. During those forty days the flow would have filled a triangular volume about 200 n mi wide by 147 n mi long by 26 fathoms deep, a total of 377 n mi or 2400 km³. This corresponds to a transport of 0.7 Sv, assuming that the entire water depth moves at the same speed. This result is somewhat lower than the 1.2 Sv estimated by Mosby (1963) but agrees as well as may be expected considering the crude assumption that the latitude of Station 23 bounds the base of the triangular area and the likelihood that the transports through Bering Strait are highly variable.

The low-salinity layer beginning at Station 23 is only 33 n mi south of the ice. This close relationship prompts the question, "Is the retreat of the ice margin somehow coupled to the flow rate through Bering Strait?". Certainly, the water cannot be advancing faster than the ice margin is retreating or the warm surface layer would be pushed under the ice. Perhaps the ice margin is retreating only as fast as the northward-flowing water melts it.

The latter idea may be explored by computing the flow rate necessary to melt 140 cm of sea ice with a layer of water at 7.6° C, 12 m deep, as at Station 23. We assume that this water moves forward uniformly as a layer, with no backward diffusion. Such motion does not really occur and the waters to the south of the ice are cooled by the diffusion of cold melt water southward. Thus, for our simple concept of motion, it is necessary to pick the temperature of a source water from a station far enough south to escape most of the effects of diffusion.

The heat of fusion of sea ice depends upon the the assumed temperature of the ice and its salinity when melting begins. The conditions assumed are ice temperature and salinity, -2° C and 4 o/oo; terminal water salinity, 30 o/oo, whence the heat of fusion is 70.8 cal/gm. The resulting requirement for water flow to melt the ice is 0.82 times the rate of retreat of the ice. Therefore, there is sufficient heat in the advancing water near 68° - 30' N to melt the ice without considering the contribution of direct insolation on the ice sheet.

Farther north (in August) the mean northward velocity of water would be expected to decrease as the Chukchi Sea widens. Yet the rate of retreat of the ice commonly is greater in August than in July, indicating that the effects of insolation, both directly on the ice and on the waters to the south, are becoming increasingly important. One would then expect the zone of melt water south of the ice to widen. The results of MIZPAC 71 and MIZPAC 72 seem to confirm this idea.

It is conceivable that the ice margin controls the northward flow and some of the phenomena at the ice margin to be discussed later suggest this. The cause could be the lateral pressure of the considerable dynamic hill which develops between Bering Strait and the ice margin as a result of the melting of ice, about 6 dyn. cm.

The bottom water on the east side of Bering Strait, rather imperfectly represented by Station 18, was at 0.05° C and 33.0 o/oo, saline enough but not cold enough to form the bottom water at Station 23. However, the water at Bering Strait likely was colder at an earlier date. But, it is not justifiable to conclude that because such water

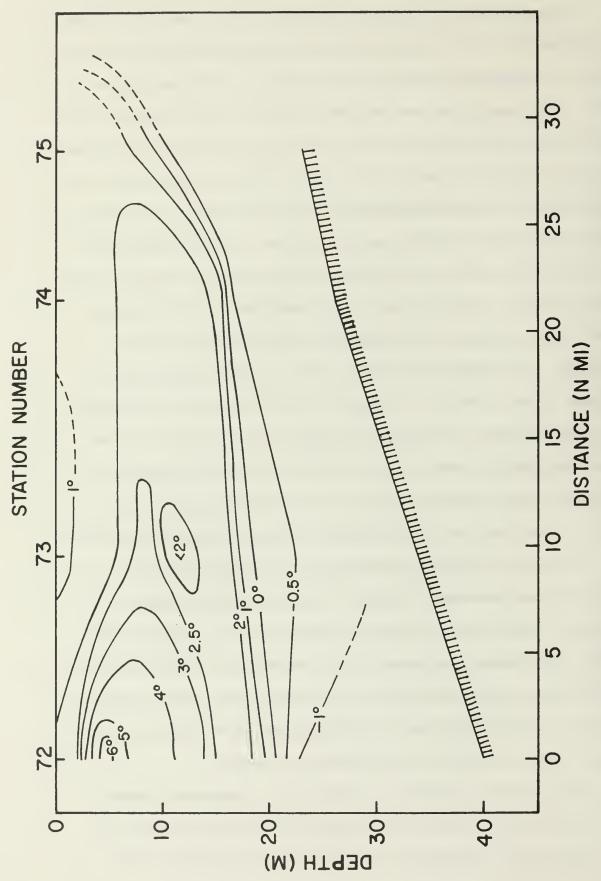
was available that it was the source water for the lower layer in the Chukchi Sea. Between Station 23 and Station 30, only 13 n mi to the north, the temperature of the bottom water drops from -1.2 to -1.72° C, an abrupt change which destroys any continuity which might have been presumed to exist because of a regular flow of bottom water northward. Evidently, an abrupt modification of bottom water is taking place near the ice margin. The bottom water under the ice, with the temperature below -1.7° C and salinity ordinarily greater than 33.0 o/oo, must have been in place before the retreat of the ice margin began north of Bering Strait. It may have been supplied earlier in the year through Bering Strait or it may have been formed in situ by freezing and the resulting convective overturn. The freezing point of water with a salinity of 33.0 is -1.80°C. slightly warmer water which is observed can have been formed by mixing between a more saline water at the equilibrium freezing temperature and a less saline water slightly warmer than the freezing temperature. The under-ice bottom water is near freezing, as one can see; thus it must have been formed by winter overturn, but that process can have occurred south of Bering Strait as well as in the Chukchi Sea.

Before considering the processes at the ice margin it is appropriate to complete the discussion of general oceanography, principally with reference to the character of the coastal current, and to make some estimate of the comparability of the 1974 data with earlier data.

Two crossings of the coastal region were made, one the sequence of Stations Nos. 72-75, and the other, Stations 89-94 and 102. Temperature cross-sections along these two lines are shown as Figures 4 and 5. The warmth which was expected along the coast is lacking, and a warm core of water appears to be centered beyond the stations farthest seaward, which are 40 n mi from the nearest shore. However, water of intermediate warmth extends shoreward below the surface, essentially to the most shoreward station in both figures. Figure 6 shows the horizontal distribution of the maximum temperature in the water column. This figure also indicates that to the south the warm core is more than 40 n mi from shore in latitudes between 68° 30' N to 70° N. In August 1971 Paquette and Bourke (1973) found the warmth closer to shore north of 70° 30'. It will be seen in Figure 6 that evidence of a similar warmth, a pocket of 3° water, is present close to the coast near that latitude. Thus, considering the earlier dates and consequent more southerly extent of the ice in the present cruise, it would seem that 1974 is not grossly different in character from 1971.

One cannot help being impressed by the westward extent of relatively warm water and question if this can all be supplied through the narrow eastern margin of Bering Strait. In view of the earlier calculations the answer to this is negative. Insolation must be the major cause for the warmth in the upper layer. The cold flow along the Russian coast also is strikingly narrow and seems to have a minor effect on the bulk of the Chukchi Sea water.

While we have a tendency to identify the temperature maximum with the core of a current, the reader will realize that this need not always be so. Shorefast ice which was more prevalent in 1974



Temperature cross-section, Stations 72-75, across the coastal current. Figure 4.

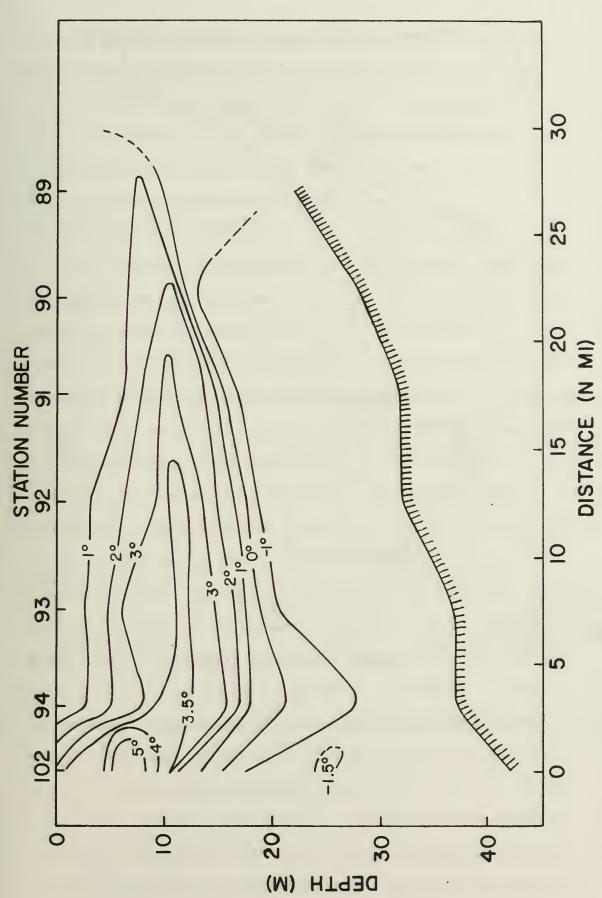


Figure 5. Temperature cross-section, Stations 89-94 and 102, across the coastal current.

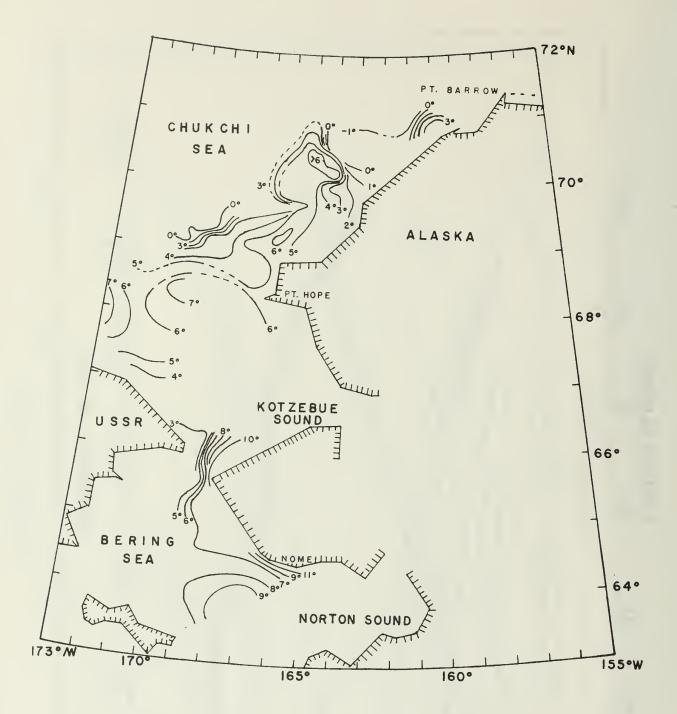


Figure 6. Map of maximum temperature in the water column.

than 1971 could, for example, have cooled the shoreward side of a warm current to yield the kind of temperature distribution shown.

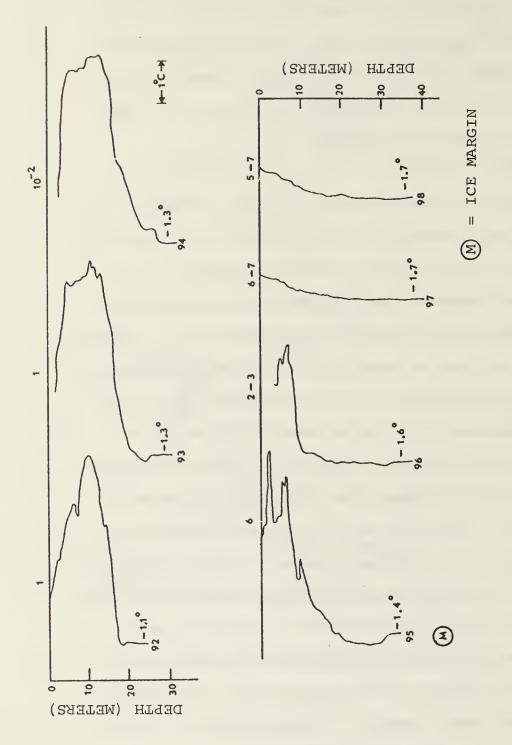
There are a number of interesting questions related to the general oceanography of the Chukchi Sea, requiring more data or extensive analysis, which will be treated at a later date. These will be mentioned under Recommendations.

B. MESOSTRUCTURE

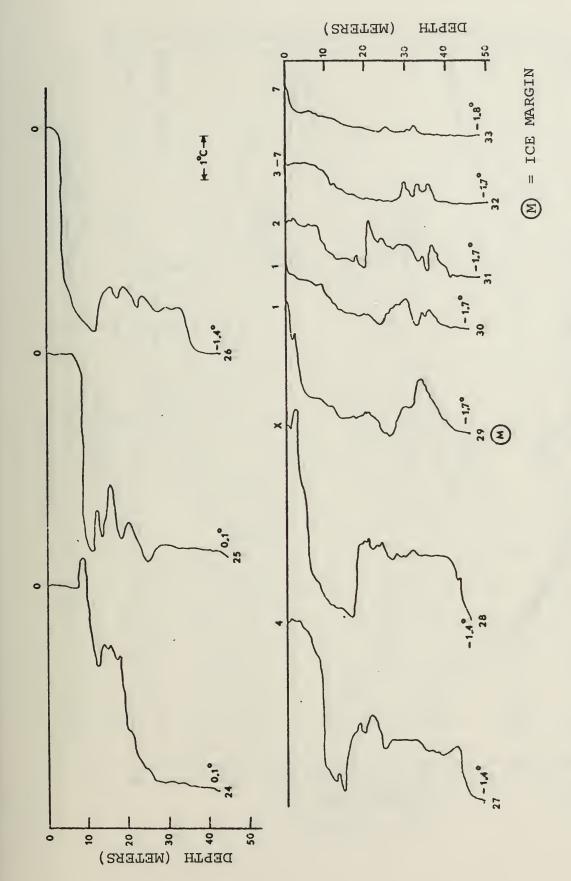
The character of the mesostructure may best be examined from the seven ice margin crossings. The first three of these contained moderate mesostructure below about 15-20 m depth whereas the remaining four had temperature profiles dominated by a shallow warm subsurface maximum with weak mesostructure in and near it. Crossings 1 and 6, which are taken as examples of the two kinds of conditions, are shown as nested temperature profiles in Figures 7 and 8. The profiles are separated by an integral number of degrees and the station number and the deepest temperature are shown at the bottom. The ice concentration is shown at the top, either in oktas or in exponential form. Temperature profiles and cross-sections of temperature and sigma-t for the other crossings are shown in Appendix IV.

Figures 9 through 12 are, respectively, temperature and sigma-t cross-sections along the line of stations in Crossings 1 and 6.

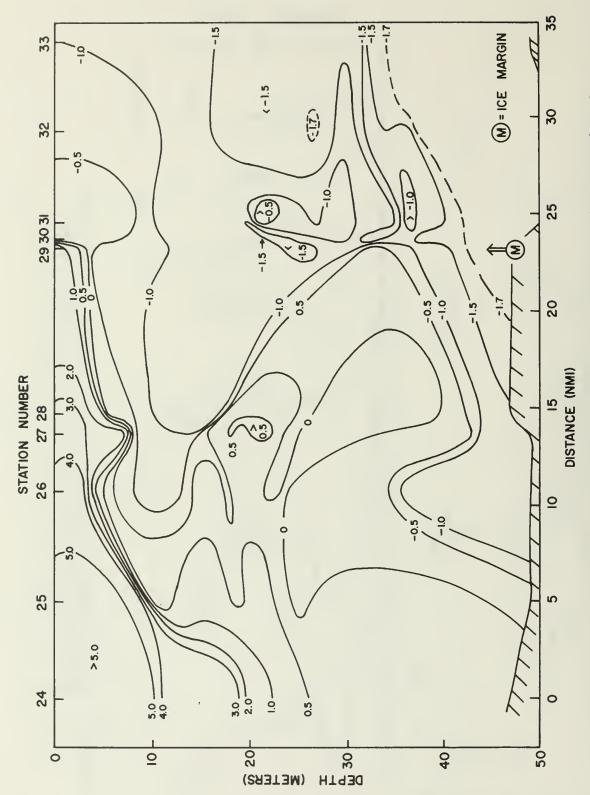
The temperatures of Crossing 1 show on the left (south) the warm near-surface water typical of the area 10 or more n mi south of the ice. Further north, Crossing 1 is characterized by a complex temperature structure, warm water near the surface above a sharp thermocline, a tongue of cold water extending toward the south (left) at 5-20 m depth and an intrusion of warm water below 20 m depth which



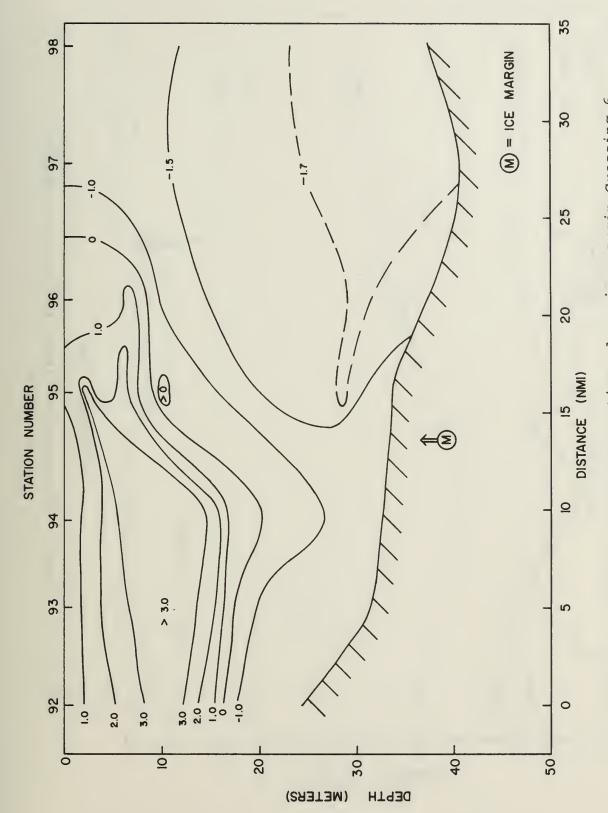
Nested temperature profiles for ice-margin Crossing 1 Numbers at the top of trace are ice concentrations; at the bottom of the trace the bottom temperature. Figure 7.



Nested temperature profiles for ice-margin Crossing 6. Numbers at the top of trace are ice concentrations; at the bottom of the trace the bottom temperature. Figure 8.



Temperature cross-section along ice-margin Crossing 1. Figure 9.



Temperature cross-section along ice-margin Crossing 6. Figure 10.

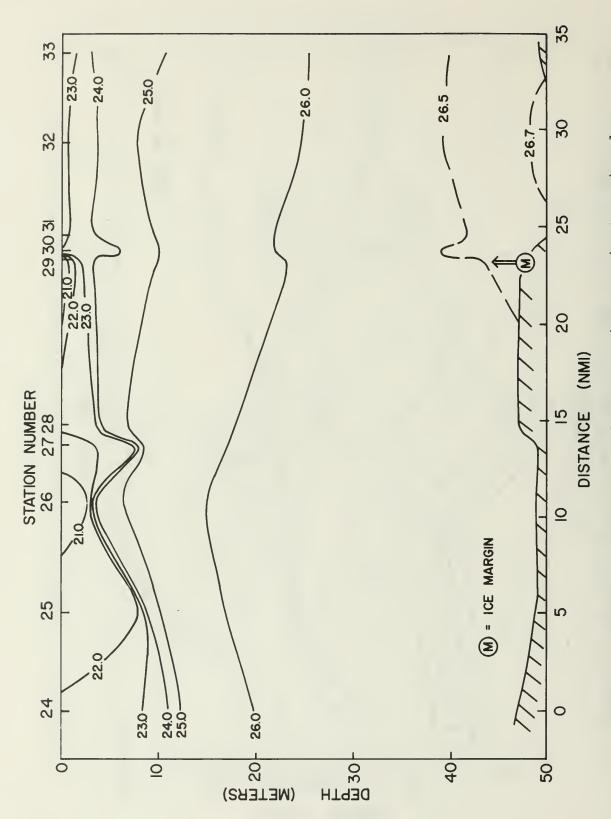
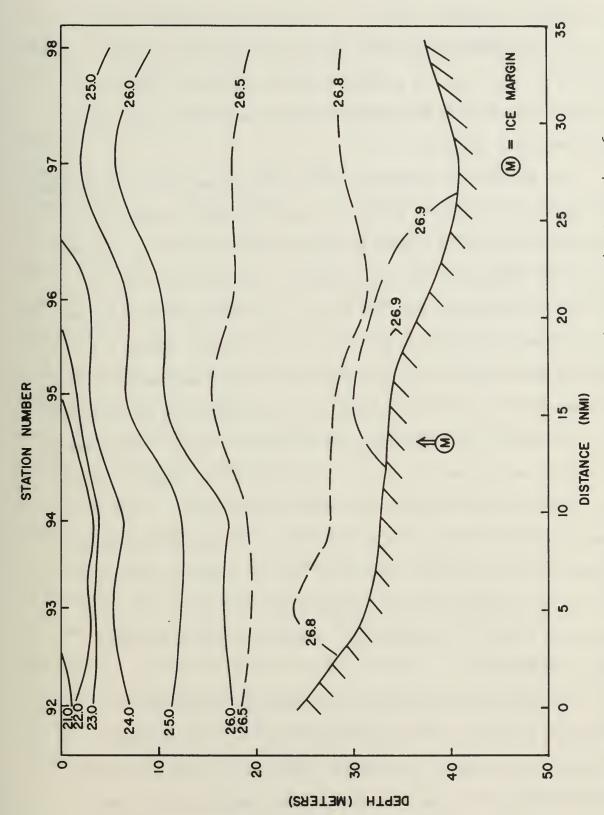


Figure 11. Sigma-t cross-section along ice-margin Crossing 1.



Sigma-t cross-section along ice-margin Crossing 6. Figure 12.

has warmed or displaced the -1.7° C water which is present deeper in the ice. In Crossing 6 the upper warm layer appears as a tongue more than 20 m thick; there is a relatively weak thermocline beneath this tongue and the section has generally a much less complex temperature structure than Crossing 1.

The densities in Crossing 1 show a sharp pycnocline corresponding to the sharp thermocline, relatively rapid changes of density in the horizontal and notable pockets of low-density water near the surface. At the low temperatures involved, density is dependent mainly on salinity so low density near the surface represents admixture of low-salinity water from melting ice. The vertical density gradient at depths greater than 20 m is relatively low. A maximum sigma-t of 26.7 corresponds to the coldest water seen in the temperature cross-section.

The densities of Crossing 6 are different. There is much less low-density water near the surface; the densities at comparable depths are higher throughout the section and the bottom water is about 0.2 sigma-t units more dense than in Crossing 1. The vertical gradient of density near the surface is smaller than in Crossing 1, but below 15 m in the southern part it is considerably greater. In the north even the 5 m depth is included in a rather low gradient from that depth to bottom.

The difference between these two crossings corresponds to a difference in intensity of the processes involved. In Crossing 1, the upper layer appears to be driven toward the ice with sufficient velocity to mix melt-water downward and heat upward; much of the subsurface heat is utilized in melting the ice and the long wedge

of decreasing temperature consequently lies mostly outside the ice margin. Melting is taking place near the nose of the wedge where there is a pronounced lateral thermal gradient.

Beneath the warm wedge is a sharp thermocline and pycnocline which probably exists because there is a lower depth limit to the mixing processes set by the gravitational forces of the vertical density gradient. Further evidence of a relatively rapid flow toward the ice is the relatively low densities, compared with Crossing 6, in the upper layer of the ice-covered portion, indicating that diluted water is being pushed under the ice. The relatively high densities which would be expected in the upper layer south of the ice, if the flow were rapid, are obscured in Crossing 1 by a local melting process going on near Station 27 due to the presence of a patch of ice of 4 oktas concentration. The expected higher densities may be seen clearly in Crossing 2 (Appendix IV).

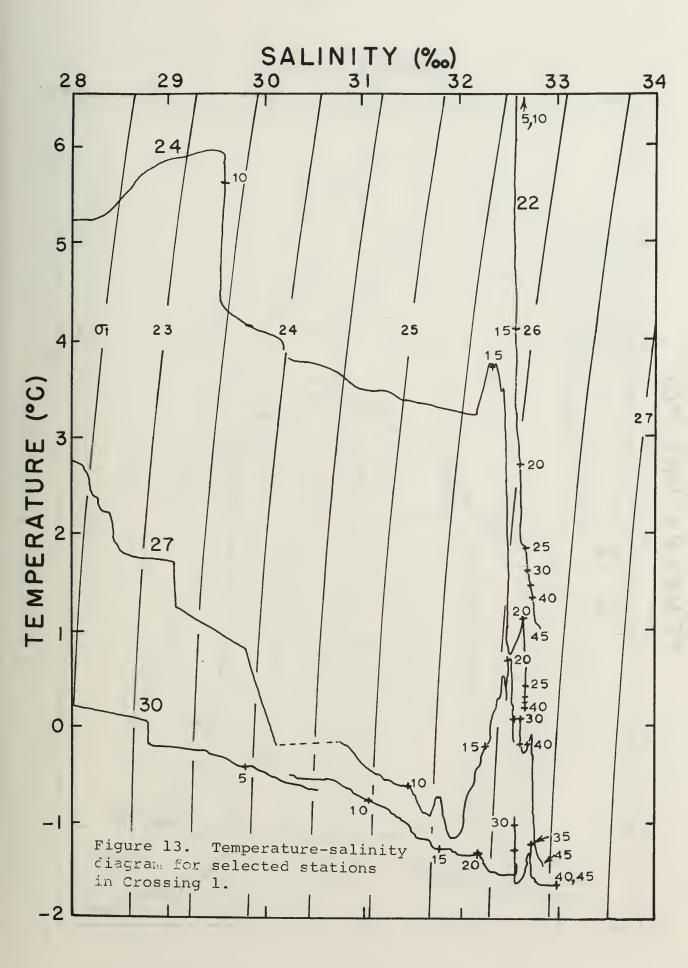
In Figures 7 and 9 the warm layers, as they enter the plotted sections, have already mixed to some degree with the deeper layer to destroy any sharp interface which may once have existed. However, in Crossing 6 the mixing has been much less extensive since the vertical density gradients are large. Furthermore, the densities near bottom are substantially greater in Crossing 6, indicating not only that vertical mixing is weaker, but also that lateral mixing of southerly bottom water into the area is weak. These are further evidences of relatively weak northerly flows.

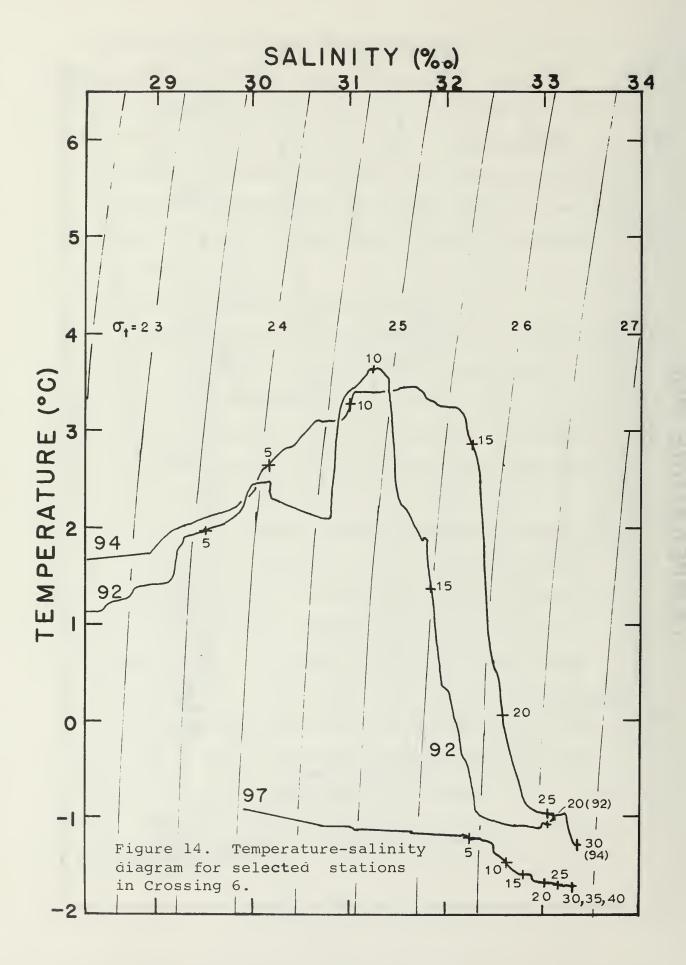
Another distinction to be drawn between Crossings 1 and 6 is in the character of the mesostructure. In Crossing 1 there is principally deep mesostructure which Corse (1974) identified in MIZPAC 71 data and defined as mesostructure occurring at a sigma-t greater than 25.5. Karrer (1975), working with MIZPAC 74 data found the same kinds under similar circumstances but put the boundary between the two at 26.0 sigma-t. Crossing 6 has essentially only shallow mesostructure in and near the warm nose.

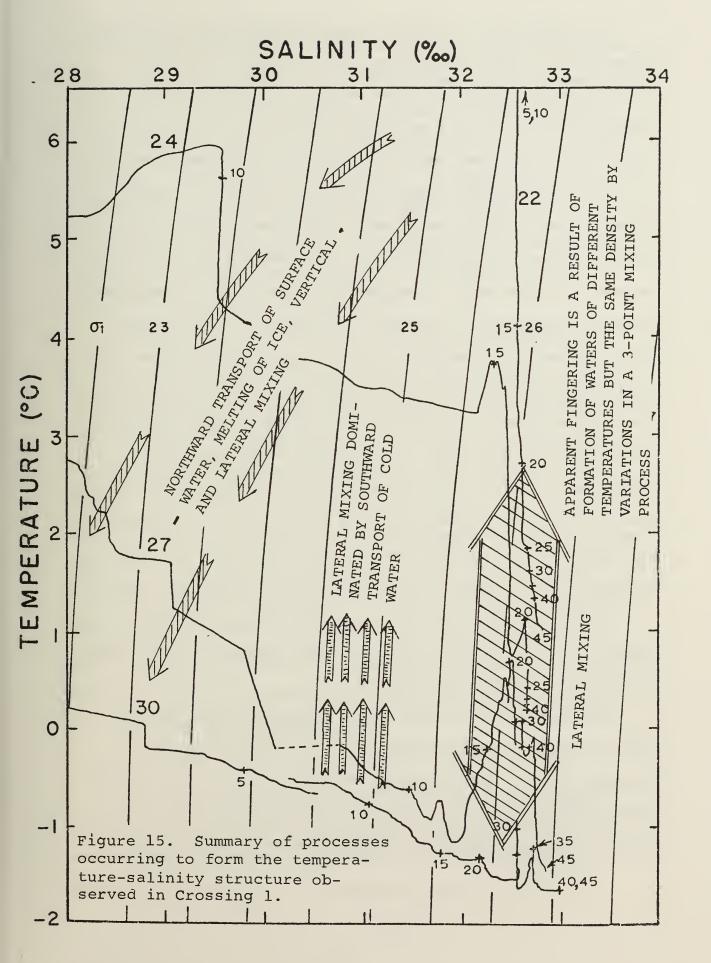
C. LATERAL MIXING PROCESSES NEAR THE ICE MARGIN

The mesostructure elements are anomalously warm lenses of water of a density appropriate to their positions at various depths in the water column. Hence, they must have part of their origin in warm surficial water or in deeper warm water to the south. As discussed below, deep structure appears to result primarily from lateral mixing of waters similar in density but different in temperature.

Figures 13 and 14 present the temperature-salinity relation for a sampling of stations in Crossings 1 and 6. A study of these diagrams gives some insight into the processes occurring, processes which are summarized graphically for Crossing 1 in Figure 15. There is little question that the warm water near the surface, upon encountering the ice, melts it and is cooled and diluted by the latent heat of freezing and the resulting melt water. A certain amount of vertical mixing must go on due to turbulence generated by ice keels interacting with flowing water which is presumed to have a component of flow toward the north. This can be seen in the decrease in density in Station 24 at depths shallower than 15 m.







The mesostructure occurs in a temperature peak which can be seen to have begun to develop at Station 24 at 15 m depth. The peak is in the vicinity of the 26.0 sigma-t surface. It exists as a peak because the water between 8 and 15 m has become colder than the water below. This cooler water must be cooled basically by lateral mixing with colder water farther under the ice as at Station 30. Vertical mixing with surficial cold water would produce water which is too dilute. Vertical mixing with the cold bottom water must be ruled out because the process would be everywhere intercepted by the temperature maximum in between which would have to disappear if cold water were mixed up through it. Therefore, one is forced to the conclusion that lateral mixing is involved. The preponderance of cold water in the mixture must be due to a transport of cold northern water southward within the 8-15 m depth band. It is a matter of relative motion. Probably more likely is the assumption that flow above and below is more rapidly northward than in the 8-15 m band. A possible cause of the relative southerly flow below the thermocline is the baroclinic lateral pressure gradient which results from the admixed melt water.

From 15 m down it appears that lateral mixing along density surfaces at about a uniform rate can account adequately for the change of properties throughout the section.

Deep mesostructure is most easily envisioned as due to horizontal mixing along density surfaces. Dense, sufficiently warm, water is present in the lower layer some miles south of the ice. To produce mesostructure it has only to mix horizontally into the cold water of the same density under and near the ice in such a way as to

cause mixing to be grossly irregular at different depths or at different places short distances away. The moderate complexity of lateral pressure gradients might be sufficient to account for the irregularity. Or, an anomalously warm water of the same density could easily be present only a short distance away, adjacent to the oceanographic section which was measured, due to the irregularity of the ice margin, particularly if the margin is diffuse. Thus, the complexity of the temperature profile may be due more to an irregularity of the ice margin than to a complexity of the lateral mixing process.

It has occurred to us that mesostructure may not be greatly different in nature from the microstructure which frequently is found in salinity-temperature-depth recorder profiles in more southerly oceans. There the amplitudes of temperature fluctuation which can result from the mixing of two water masses are limited by the relatively small density changes which can be brought about during mixing and the relatively large area in which the density-temperature correlation is almost the same. At low temperatures, density and temperature are weakly correlated and, near the ice margin, the density-temperature relationship changes markedly within a few miles. Thus, if similar interleaving occurs in the two situations, the temperature amplitude of the anomaly can be much larger in the Chukchi Sea than in more southerly oceans.

IV. CONCLUSIONS AND RECOMMENDATIONS

A. CONCLUSIONS

In MIZPAC 74 seven ice-margin crossings with closely spaced stations were made, three of which showed deep temperature mesostructure and four did not. Those which did not tended to show a shallow warm protuberance in the temperature profile called the

"warm nose" and upon and near this nose was shallow mesostructure (sigma-t less than 25.5 to 26.0). It appears that the crossings having deep mesostructure were associated with a strong flow of warm southerly water toward the ice whereas those having the warm nose and shallow mesostructure had a weaker flow toward the ice. In the former case there appeared to be an internal vertical circulation which recirculated a cold, somewhat diluted water southward in the upper middepth.

It is proposed that deep mesostructure is due to a lateral mixing process in mid-depth between a warmer southerly water and a cold under-ice water, both of nearly the same density. Temperature anomalies then result, perhaps by uneven mixing longitudinally along the direction of presumed water flow. Or, because of the irregularity of the ice margin, different mixtures may be formed at points closely adjacent to the section under measurement (hence not visible); these may then interleave under conditions requiring little lateral movement and nearly no work to be done against density forces.

It is suggested that the mesostructure of the Chukchi Sea may be analogous to some of the microstructure seen in more southerly oceans but has larger temperature amplitudes because the density-temperature relation changes so markedly over short distances in the Chukchi Sea.

Some of the general oceanography of the region north of Bering Strait has been discussed. In particular, it is found that a fairly well-defined margin, north of which there is an upper, low-salinity layer, probably marks the boundary of ice-melt water pushed northward

by the flow through Bering Strait. Further, it seems evident that both bottom water and surface water are being modified at the ice margin as the ice retreats. One must therefore use caution in tracing water types along paths which cross the ice margin. It appears that the advancing Bering Sea water is moving northward at about the same rate as the ice margin is retreating. One speculates that processes at the ice margin may control the northward flow, perhaps by means of the dynamic hill generated in the north by the melting of ice.

B. RECOMMENDATIONS

Based upon the observations and results from the three MIZPAC cruises to date there appear to be several major features relating to the character and formation of mesostructure that require explanation and further investigation in the field. For some of these features only generalizations can be inferred; the degree of variability, both temporally and spatially, may be largely unknown. For other features, e.g., the degree of compactness of the ice edge, few measurements exist, as their importance relative to mesostructure formation has only recently come to light. Some topics or features that need further investigation are:

- The occurrence of mesostructure in general. We have too few examples upon which to draw definitive conclusions.

 The effects of location and of season also are of interest.
- The presence of deep mesostructure in some cases and shallow mesostructure in others.
- The mixing processes occurring, particularly those at middepth, which create the deep mesostructure elements.

- The mechanism for the apparent southward flow of cool water at about 12-15 m depth, <u>viz</u>, Crossing 1, which leaves the peaks of mesostructure outstanding. This should be confirmed by direct current measurements.
- The presence and relative strength of mesostructure with regard to compactness of the ice edge.
- The relation between mesostructure strength and currents at the ice edge, especially the flow characteristics relative to the orientation of the ice edge.
- The relative position and warmth of the coastal current and its effect on mesostructure formation.
- The three-dimensional distribution of water properties in areas with mesostructure.
- The occurrence of mesostructure in waters distant (20-40 n mi) from the ice edge.
- The coupling between northward water flow and the retreat of the ice margin.
- The question of bottom water, its origins and modifications.
- Quantification of the role of solar heating in the melting processes and the role of Kotzebue Sound as a heat sink.

V. ACKNOWLEDGMENTS

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Technicians of the BURTON ISLAND. Mr. Peter Becker of the Applied Physics Laboratory, University of Washington graciously provided his CTD data to aid in interpreting results when our equipment failed.

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APPENDIX I

EXPLANATION OF HEADING CODES

The heading of the printed output uses the coding and format from NODC Publication M-2, August 1964, with a few exceptions. Heading entries which are not self-explanatory are as follows. MSQ is the Marsden Square, DPTH is the water depth in meters, OBS is the number of observations in the tabulation. Wave source direction is in tens of degrees, but the direction 99 indicates no observation. significant wave height is coded by Table 10 (Code + 2 & height in meters) and the wave period coded by Table 11 (Code $\div 2\%$ period in sec); in each case X indicates no observation. Wind speed, V, is coded as Beaufort force, Table 17. The barometer is in millibars, less 1000 if more than 3 digits; wet and dry bulb temperatures are in degrees C. The present weather is from Table 21 with cloud type and amount from Tables 25 and 26, respectively. The combination 4 X 9 indicates that clouds cannot be observed usually because of fog conditions. The visibility is from Table 27 which is roughly in powers of two with Code 4 = 1-2 km. The ice concentration, IC, is in oktas; amounts less than 1 okta are preceded by a minus sign and indicate concentrations in powers of ten, e.g., $10^{-4} = -4$.

The entry, COD, is a code to identify the method of observation taken on station: Code 1 indicates an STD observation, Code 2 a CTD observation, and Code 3 an XBT (temperature only) observation. SORD indicates a shallow shunted (S) STD lowering while D indicates a deep non-shunted STD lowering.

APPENDIX II

STD HEADING DATA AND PROPERTY PROFILES

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	:	14-17	II	-12	
	:	18-21	II	-13	
	:	22-25	II	-14	
	:	26-29	II	-15	
	:	30-33	II	-16	
	:	34-37	II	-17	
	:	38-40, 42	II	-18	
	:	43-46	II	-19	
	:	47-50	II	-20	
	:	51-54	II	-21	
	:	55-58	II	-22	
	:	59-62	II	-23	
	:	63-66	II	-24	
	:	67-70	II	-25	
	:	71-74	II	-26	
	:	75-77,77A	II	-27	
	:	78-81	II	-28	
	:	82-85	II	-29	
	:	86-89	II	-30	
	:	90-93	II	-31	
	:	94-97	II	-32	
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COD		-	-	~	_	1	-	1	1	~	1	~	1	~	1	-	1	-	1	-	-
JBS		2.0	960	754	716	702	152	106	714	106	140	113	869	108	108	660	969	407	082	112	681
																				0.1	
DPTH		29	57	57	54	54	54	54	54	54	54	54	54	54	54	54	54	54	54	52	52
STA DPTH	6	0328	0338	0330	034	0350	0358	0368	0360	0370	0378	0388	0380	0380	8660	0408	0400	0420	0428	0438	0430
	6	0328							0360		0378	0388	0380		8660	0408					
HP STA	6	10.8 0325	12.2 0335	12.2 0330	19.0 034	20.1 0350	20.1 0355	21.6 0365	21.6 036D	23.7 0370	23.7 0375	00.7 0385	00.7 038D	01.7 0390	01.7 0395	02.8 0408	05.8 0400	05.6 0420	05.6 0425	12.6 0435	12.6 0430
HP STA	6	10.8 0325	12.2 0335	12.2 0330	19.0 034	20.1 0350	20.1 0355	21.6 0365	21.6 036D	23.7 0370	23.7 0375	00.7 0385	19 74 00.7 0380	01.7 0390	01.7 0395	02.8 0408	05.8 0400	05.6 0420	19 74 05.6 9428	12.6 0435	12.6 0430
MO DY YP HP STA		07 18 74 10.8 0325	07 18 74 ,12.2 0335	07 18 74 12.2 0330	07 18 74 19.0 034	07 18 74 20.1 0350	07 18 74 20.1 0355	07 18 74 21.6 0365	07 18 74 21.6 036D	07 18 74 23.7 0370	07 18 74 23.7 0375	07 19 74 00.7 038S	07 19 74 00.7 0380	07 19 74 01.7 0390	07 19 74 01.7 0395	07 19 74 02.8 0408	07 19 74 02.8 0400	07 19 74 05.6 0420	07 19 74 05.6 0428	07 19 74 12.6 0435	07 19 74 12.6 0430
HP STA		10.8 0325	12.2 0335	12.2 0330	19.0 034	20.1 0350	20.1 0355	21.6 0365	21.6 036D	23.7 0370	23.7 0375	00.7 0385	19 74 00.7 0380	01.7 0390	01.7 0395	02.8 0408	05.8 0400	05.6 0420	19 74 05.6 9428	12.6 0435	12.6 0430
MSQ MQ DY YP HP STA		234 07 18 74 10.8 0325	234 07 18 74 ,12.2 0335	234 07 18 74 12.2 0330	233 07 18 74 19.0 034	233 07 18 74 20.1 035D	233 07 18 74 20.1 0355	233 07 18 74 21.6 0365	233 07 18 74 21.6 036D	233 07 18 74 23.7 0370	233 07 18 74 23.7 0375	233 07 19 74 00.7 038S	233 07 19 74 00.7 0380	233 07 19 74 01.7 0390	233 07 19 74 01.7 0395	233 07 19 74 02.8 040S	233 07 19 74 02.8 0400	233 07 19 74 05.6 0420	233 07 19 74 05.6 0428	233 07 19 74 12.6 0438	233 07 19 74 12.6 0430
MSQ MQ DY YP HP STA		234 07 18 74 10.8 0325	234 07 18 74 ,12.2 0335	234 07 18 74 12.2 0330	233 07 18 74 19.0 034	233 07 18 74 20.1 035D	233 07 18 74 20.1 0355	233 07 18 74 21.6 0365	233 07 18 74 21.6 036D	233 07 18 74 23.7 0370	233 07 18 74 23.7 0375	233 07 19 74 00.7 038S	233 07 19 74 00.7 0380	233 07 19 74 01.7 0390	233 07 19 74 01.7 0395	233 07 19 74 02.8 040S	233 07 19 74 02.8 0400	233 07 19 74 05.6 0420	233 07 19 74 05.6 0428	233 07 19 74 12.6 0438	233 07 19 74 12.6 0430
MO DY YP HP STA		170-61.7 234 07 18 74 10.8 0328	170-03.5 234 07 18 74 12.2 0338	170-03.5 234 07 18 74 12.2 0330	169-06.0 233 07 18 74 19.0 034	169-02.8 233 07 18 74 20.1 0350	169-02.8 233 07 18 74 20.1 0355	169-06-1 233 07 18 74 21.6 0365	169-06.1 233 07 18 74 21.6 036D	169-06.0 233 07 18 74 23.7 0370	169-06.0 233 07 18 74 23.7 0375	169-06.C 233 07 19 74 00.7 038S	169-06.0 233 07 19 74 00.7 0380	169-60.0 233 07 19 74 01.7 0390	169-00.0 233 07 19 74 01.7 0395	168-55.1 233 07 19 74 02.8 0408	168-55.1 233 07 19 74 02.8 0400	168-55.1 233 07 19 74 05.6 0420	168-55.1 233 07 19 74 05.6 0428	167-36.5 233 07 19 74 12.6 0438	167-36.5 233 07 19 74 12.6 0430
LCNG MSQ MQ DY YP HP STA		170-61.7 234 07 18 74 10.8 0328	170-03.5 234 07 18 74 12.2 0338	170-03.5 234 07 18 74 12.2 0330	169-06.0 233 07 18 74 19.0 034	169-02.8 233 07 18 74 20.1 0350	169-02.8 233 07 18 74 20.1 0355	169-06-1 233 07 18 74 21.6 0365	169-06.1 233 07 18 74 21.6 036D	169-06.0 233 07 18 74 23.7 0370	169-06.0 233 07 18 74 23.7 0375	169-06.C 233 07 19 74 00.7 038S	169-06.0 233 07 19 74 00.7 0380	169-60.0 233 07 19 74 01.7 0390	169-00.0 233 07 19 74 01.7 0395	168-55.1 233 07 19 74 02.8 0408	168-55.1 233 07 19 74 02.8 0400	168-55.1 233 07 19 74 05.6 0420	168-55.1 233 07 19 74 05.6 0428	167-36.5 233 07 19 74 12.6 0438	167-36.5 233 07 19 74 12.6 0430
LCNG MSQ MQ DY YP HP STA		170-61.7 234 07 18 74 10.8 0328	170-03.5 234 07 18 74 12.2 0338	170-03.5 234 07 18 74 12.2 0330	169-06.0 233 07 18 74 19.0 034	169-02.8 233 07 18 74 20.1 0350	169-02.8 233 07 18 74 20.1 0355	169-06-1 233 07 18 74 21.6 0365	169-06.1 233 07 18 74 21.6 036D	169-06.0 233 07 18 74 23.7 0370	169-06.0 233 07 18 74 23.7 0375	169-06.C 233 07 19 74 00.7 038S	169-06.0 233 07 19 74 00.7 0380	169-60.0 233 07 19 74 01.7 0390	169-00.0 233 07 19 74 01.7 0395	168-55.1 233 07 19 74 02.8 0408	168-55.1 233 07 19 74 02.8 0400	168-55.1 233 07 19 74 05.6 0420	168-55.1 233 07 19 74 05.6 0428	167-36.5 233 07 19 74 12.6 0438	167-36.5 233 07 19 74 12.6 0430
LCNG MSQ MQ DY YP HP STA		234 07 18 74 10.8 0325	234 07 18 74 ,12.2 0335	234 07 18 74 12.2 0330	233 07 18 74 19.0 034	233 07 18 74 20.1 035D	233 07 18 74 20.1 0355	233 07 18 74 21.6 0365	233 07 18 74 21.6 036D	233 07 18 74 23.7 0370	233 07 18 74 23.7 0375	233 07 19 74 00.7 038S	233 07 19 74 00.7 0380	233 07 19 74 01.7 0390	233 07 19 74 01.7 0395	233 07 19 74 02.8 040S	233 07 19 74 02.8 0400	233 07 19 74 05.6 0420	233 07 19 74 05.6 0428	233 07 19 74 12.6 0438	233 07 19 74 12.6 0430
MSQ MQ DY YP HP STA		170-61.7 234 07 18 74 10.8 0328	170-03.5 234 07 18 74 12.2 0338	170-03.5 234 07 18 74 12.2 0330	169-06.0 233 07 18 74 19.0 034	169-02.8 233 07 18 74 20.1 0350	169-02.8 233 07 18 74 20.1 0355	169-06-1 233 07 18 74 21.6 0365	169-06.1 233 07 18 74 21.6 036D	169-06.0 233 07 18 74 23.7 0370	169-06.0 233 07 18 74 23.7 0375	169-06.C 233 07 19 74 00.7 038S	169-06.0 233 07 19 74 00.7 0380	169-60.0 233 07 19 74 01.7 0390	169-00.0 233 07 19 74 01.7 0395	168-55.1 233 07 19 74 02.8 0408	168-55.1 233 07 19 74 02.8 0400	168-55.1 233 07 19 74 05.6 0420	168-55.1 233 07 19 74 05.6 0428	167-36.5 233 07 19 74 12.6 0438	167-36.5 233 07 19 74 12.6 0430

SORD					٥	S	S	0	0	S	S	٥	0	S		0	S			
VIS		9			80	œ										œ	00	œ	9	9
AMT		œ			80	00									œ	80	œ	œ	80	
CL CL		7			7	7										7	7	7	7	
WTHP		2			2	2									9	2	2	2	7	
WET		01.4	01.1	6.00											01.6			8.00		
DRY															01.8			6.00		
BAR	004	900											600	600		010	010			
>	m	m		3											2			2	-	0
ON.	66	35	66	66	66	66	66	66	66	66	66	66	66	66	01	66	66	02	01	00
PER	×	×	×	×	×	×	×	×	×	×	×	×	×	×	×	×	×	×	×	×
Ε	×	-	×	×	0	0	0	0	×	×	×	×	×	×	-	×	×	0	0	0
MVD	66	35	66	66	00	00	66	66	66	66	66	66	66	66	66	66	66	02	01	01
0	0	0	0	-3	-3	n	0	0	m	n	5	2	2	7	0	0	0	ပ	0	0
COD	-	-	Н	-	1	-	1	1	1	1	-	7	1	-	1	-	-	-	-	-
388	099	099	699	664	658	960	043	662	664	136	140	613	949	119	545	538	860	628	614	618
DPTH	51	20	51	51	20	20	51	51	51	51	48	48	64	64	43	43	43	55	47	48
STA	044	045	940	047	0480	0485	0498	0640	0050	0508	0518	0510	0520	0528	053	0540	0548	055	950	057
å E	14.0	15.0	16.0	16.7	17.5	17.5	18.8	18.8	22.2	22.2	23.7	23.7	01.3	01.3	09.1	10.8	10.8	13.9	16.3	17.9
MO DY YR	07 19 74	07 19 74	07 19 74	07 19 74	07 19 74	07 19 74	07 19 74	07 19 74	07 19 74	07 19 74	07 19 74	07 19 74	07 20 74	07 20 74	07 20 74	07 20 74	07 20 74	97 20 74	07 20 74	07 20 74
MSQ	233	233	233	233	233	233	233	233	233	233	233	233	233	233	233	233	233	233	569	569
LONG		167-36.0	167-37.0	167-37.0	167-37.0	167-37.0	167-40.5	167-40.5	167-40.1	167-40.1	167-42.0	167-42.0	167-36.0	167-36.0	166-60.0	166-00.0	166-00.0	165-57.0	165-54.8	165-55.5
10			1	1	7-	-10	-19	-19	-19	-191	167-	167-	167-	167-	166-	-991	-991	-69	-59	-69
	167-32.0																			
LAT			69-20.0	69-21.0	69-21.8		69-23.2	69-23.2	69-27.5		69-29.4	69-29.4			69-31.9	69-43.8		0.65-69		
	31 8! 69-18.0 167-	31 81 69-19.0 167-				31 81 69-21.8 16				31 81 69-27.5			31 81 69-31.9	31 81 69-31.9			31 81 69-43.8 1		1 81 70-11.4 1	31 RI 70-21.7 1

SURD						٥	S	S	٥	0	S	0	S	S	0	۵	S	S	0	0
VIS	c o		7	9	_	80	80	4	4	4	4			9	9			9	9	9
AMT V				9				7	7	6	6			9	9			4	4	-
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E H				7				1	1	4	4			_	7				_	7
¥ ET																				
DRY																				
BAR			012			012	012	012	012					013	013			013	013	
>	0	0	0	0	7	2	2	2	2	М	т			ю	М			0	0	М
MND	00	00	00	00	36	66	66	04	04	04	0 4	66	66	66	66	66	66	00	00	0.7
PER	×	×	×	×	×	×	×	×	×	×	×	×	×	×	×	×	×	×	×	×
Ħ	0	0	0	0	0	0	0	0	0	0	0	×	×	0	0	×	×	×	×	0
MAND	01	01	00	00	00	66	66	04	04	04	04	66	66	00	00	66	66	66	66	00
1 C	0	0	-	7	4-	2	2	3	т	O	0	7	7	4-	4	0	0		_	2
CrD	-	-	-	7	-	-	7	1	7	-	7	-	-	7	-	1	1	7	7	1
088	587	328	602	588	573	587	105	112	595	535	122	548	190	055	649	537	106	111	919	593
Ö																				
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р нт чо	94	64	94	94	94	94	94	45	45	43	43	43	43	43	43	43	43	45	45	45
Нт ФО	46	64	446	94					45	43		43	43	43	43	80 43		95 45	90 45	
	058 46	650 46	94 090	061 46	062	0630	0635	0648	0640 45	0650 43	0658	0660 43	0665 43	0675 43	0670 43	0680 43	0688	0695 45	0690 45	0010
Нт ФО	46	64	446	94					45	43		43	43	43	43	12.7 0680 43		13.6 0695 45	13.6 0690 45	
HP STA DPTH	19.0 058 46	74 19.8 059 49	21.3 060 46	74 22.0 061 46	23.0 062	00.3 0630	74 00.3 0638	02.3 0645	74 02.3 0640 45	09.4 065D 43	09.4 0655	10.5 0660 43	10.5 0665 43	74 11.7 0675 43	11.7 0670 43	12.7	12.7 0685	13.6	13.6	14.7 0700
HP STA DPTH	19.0 058 46	20 74 19.8 059 49	20 74 21.3 060 46	20 74 22.0 061 46	20 74 23.0 062	21 74 00.3 0630	21 74 00.3 0635	02.3 0645	21 74 02.3 0640 45	21 74 09.4 0650 43	09.4 0655	21 74 10.5 0660 43	10.5 0665 43	21 74 11.7 0675 43	11.7 0670 43	21 74 12.7	21 74 12.7 0685	13.6	21 74 13.6	14.7 0700
MO DY YR HP STA DPTH	058 46	74 19.8 059 49	21.3 060 46	74 22.0 061 46	23.0 062	00.3 0630	74 00.3 0638	0648	74 02.3 0640 45	09.4 065D 43	0658	10.5 0660 43	0665 43	74 11.7 0675 43	0670 43	12.7	12.7 0685		07 21 74 13.6	0010
HP STA DPTH	19.0 058 46	20 74 19.8 059 49	20 74 21.3 060 46	20 74 22.0 061 46	20 74 23.0 062	21 74 00.3 0630	21 74 00.3 0635	02.3 0645	21 74 02.3 0640 45	21 74 09.4 0650 43	09.4 0655	21 74 10.5 0660 43	10.5 0665 43	21 74 11.7 0675 43	11.7 0670 43	21 74 12.7	21 74 12.7 0685	13.6	21 74 13.6	14.7 0700
MS2 MO DY YR HP STA DPTH	269 07 20 74 19.0 058 46	269 07 20 74 19.8 059 49	269 07 20 74 21.3 060 46	269 07 20 74 22.0 061 46	269 07 20 74 23.0 062	269 07 21 74 00.3 0630	269 07 21 74 00.3 0638	269 07 21 74 02.3 0645	269 07 21 74 02.3 0640 45	269 07 21 74 09.4 0650 43	269 07 21 74 09.4 0655	269 07 21 74 10.5 0660 43	269 07 21 74 10.5 0665 43	269 07 21 74 11.7 3675 43	269 07 21 74 11.7 0670 43	269 07 21 74 12.7	269 07 21 74 12.7 0685	269 07 21 74 13.6	269 07 21 74 13.6	269 07 21 74 14.7 0700
MO DY YR HP STA DPTH	07 20 74 19.0 058 46	07 20 74 19.8 059 49	07 20 74 21.3 060 46	07 20 74 22.0 061 46	07 20 74 23.0 062	07 21 74 00.3 0630	07 21 74 00.3 0635	07 21 74 02.3 0645	07 21 74 02.3 0640 45	07 21 74 09.4 0650 43	07 21 74 09.4 0655	07 21 74 10.5 0660 43	07 21 74 10.5 0665 43	07 21 74 11.7 0675 43	07 21 74 11.7 067D 43	07 21 74 12.7	07 21 74 12.7 0685	07 21 74 13.6	07 21 74 13.6	07 21 74 14.7 0700
LENG MS MO DY YR HP STA DPTH	165-53.6 269 07 20 74 19.0 058 46	165-56.0 269 07 20 74 19.8 059 49	165-52.9 269 07 20 74 21.3 060 46	165-56.5 269 07 20 74 22.0 061 46	165-56.2 269 07 20 74 23.0 062	165-59.0 269 07 21 74 00.3 0630	165-59.0 269 07 21 74 00.3 0638	165-58.4 269 07 21 74 02.3 0645	165-58.4 269 07 21 74 02.3 0640 45	164-24.8 269 07 21 74 09.4 0650 43	154-24.8 269 07 21 74 09.4 0655	164-24.6 269 07 21 74 10.5 0660 43	164-24.6 269 07 21 74 10.5 0665 43	164-24.5 269 07 21 74 11.7 3675 43	164-24.5 269 07 21 74 11.7 0670 43	164-28.0 269 07 21 74 12.7	164-28.0 269 07 21 74 12.7 0685	164-28.4 269 07 21 74 13.6	164-28.4 269 07 21 74 13.6	164-28.C 269 07 21 74 14.7 070D
LENG MS MO DY YR HP STA DPTH	165-53.6 269 07 20 74 19.0 058 46	70-24.0 165-56.0 269 07 20 74 19.8 059 49	70-26.5 165-52.9 269 07 20 74 21.3 060 46	70-27.7 165-56.5 269 07 20 74 22.0 061 46	70-28.9 165-56.2 269 07 20 74 23.0 062	70-22.3 165-59.0 269 07 21 74 00.3 0630	70-32.3 165-59.0 269 07 21 74 00.3 0638	165-58.4 269 07 21 74 02.3 0645	70-36.8 165-58.4 269 07 21 74 02.3 0640 45	70-21.5 164-24.8 269 07 21 74 09.4 0650 43	70-21.5 154-24.8 269 07 21 74 09.4 0655	76-22.4 164-24.6 269 07 21 74 10.5 0660 43	70-22.4 164-24.6 269 07 21 74 10.5 0665 43	70-26.0 164-24.5 269 07 21 74 11.7 3675 43	164-24.5 269 07 21 74 11.7 0670 43	70-26.0 164-28.0 269 07 21 74 12.7	7C-26.0 164-28.0 269 07 21 74 12.7 068S	70-28.0 164-28.4 269 07 21 74 13.6	70-28.0 164-28.4 269 07 21 74 13.6	70-31.0 164-28.C 269 07 21 74 14.7 070D
LENG MS MO DY YR HP STA DPTH	269 07 20 74 19.0 058 46	165-56.0 269 07 20 74 19.8 059 49	165-52.9 269 07 20 74 21.3 060 46	165-56.5 269 07 20 74 22.0 061 46	165-56.2 269 07 20 74 23.0 062	165-59.0 269 07 21 74 00.3 0630	165-59.0 269 07 21 74 00.3 0638	269 07 21 74 02.3 0645	165-58.4 269 07 21 74 02.3 0640 45	164-24.8 269 07 21 74 09.4 0650 43	154-24.8 269 07 21 74 09.4 0655	164-24.6 269 07 21 74 10.5 0660 43	164-24.6 269 07 21 74 10.5 0665 43	164-24.5 269 07 21 74 11.7 3675 43	269 07 21 74 11.7 0670 43	164-28.0 269 07 21 74 12.7	164-28.0 269 07 21 74 12.7 0685	164-28.4 269 07 21 74 13.6	164-28.4 269 07 21 74 13.6	164-28.C 269 07 21 74 14.7 070D
MS2 MO DY YR HP STA DPTH	165-53.6 269 07 20 74 19.0 058 46	70-24.0 165-56.0 269 07 20 74 19.8 059 49	70-26.5 165-52.9 269 07 20 74 21.3 060 46	70-27.7 165-56.5 269 07 20 74 22.0 061 46	70-28.9 165-56.2 269 07 20 74 23.0 062	70-22.3 165-59.0 269 07 21 74 00.3 0630	70-32.3 165-59.0 269 07 21 74 00.3 0638	165-58.4 269 07 21 74 02.3 0645	70-36.8 165-58.4 269 07 21 74 02.3 0640 45	70-21.5 164-24.8 269 07 21 74 09.4 0650 43	70-21.5 154-24.8 269 07 21 74 09.4 0655	76-22.4 164-24.6 269 07 21 74 10.5 0660 43	70-22.4 164-24.6 269 07 21 74 10.5 0665 43	70-26.0 164-24.5 269 07 21 74 11.7 3675 43	164-24.5 269 07 21 74 11.7 0670 43	70-26.0 164-28.0 269 07 21 74 12.7	7C-26.0 164-28.0 269 07 21 74 12.7 068S	70-28.0 164-28.4 269 07 21 74 13.6	70-28.0 164-28.4 269 07 21 74 13.6	70-31.0 164-28.C 269 07 21 74 14.7 070D

MIZPAC 74 STD STATIONS

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SORD	S	٥	S	۵	S	S	0					<					٥	S	S	٥
VIS	9	9	9	00	∞	œ	œ	œ		∞	œ	œ	œ	00	œ	œ			80	œ
AMT	-	0	0	0	0	0	0	0		0	0	0	т	0	0	7			m	m
CL	7												7			0			7	7
WTHR	_	0	0	0	0	0	0	0		0	0	0	1	0	0	1				
WET																				
DRY																				
ВАР				41	014	41	41	41					2	40	4(004	33	3		
				0	0	0	0											003		
> Q	3	2	2	4	4		_	9		2	2		0	0	2	0	3	3		
MND	07	0	0	3	35	66	66	66	66	13	66	66	00	00	27	0	66	66	66	66
PER	×	×	×	×	×	×	×	×	×	×	×	×	×	×	×	×	×	×	×	×
Ħ	0	0	0	0	0	0	0	×	×	2	0	×	0	0	0	0	0	0	×	×
WVD	00	00	00	66	66	00	00	66	66	66	66	66	66	00	27	30	00	00	66	66
10	7	00	00	0	0	7	7	4	-2	0	0	0	0	0	0	9-	-	7	-	-
CCD	-	-	_	-	-	-	-	-	-	-	-	_		_	_	-	П	П	-	-
388	131	534	101	518	054	282	419	307	255	199	702	583	5 80	+28	t 11	413	393	920	101	396
		_		••			•	,	•••	•		-	-,	•	,	•	,		_	
DPTH	45	48	48	40	40	34	34	56	23	48	51	48	44	35	36	34	32	32	32	32
DA																				
STA	0708	071D	0718	72D	0728	738	073D	14	15	91	17	77A	810	64	080	081	082D	0825	0835	083D
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_		16	164			164			16	16		16	167	166			16		16,	164-03.4
F	BI 70-31.0	4.1	4.1	70-11.6	70-11.6	70-07	70-07	70-03.6	4.4	8.0	3.5	4.0	0.0	6.2	69-33.4	BI 69-51.6	1.2	70-01.2	70-03.8	3.8
LAT	70-3	70-34.1	70-34.1	1-0-1	1-0	0-0	0-0	0-0	3-6	67-48.0	8-2	68-34.0	8-5	69-16.2	6-6	9-6	70-01.2	0-0	0-0	0-0
SHIP	B I	81 7	BI 7	BI 7	81 7	BI 7	BI 7	BI 7	BI 69-54.4	BI 6	BI 68-23.5	BI 6	BI 68-50.0	BI 6	BI 6	BI 6	BI 7	BI 7	BI 7	BI 70-03.8
NAT SI	31	31	31	31	31	11	3.1	31	31	31	31	31	31	31	31	31	31	31	1.	31
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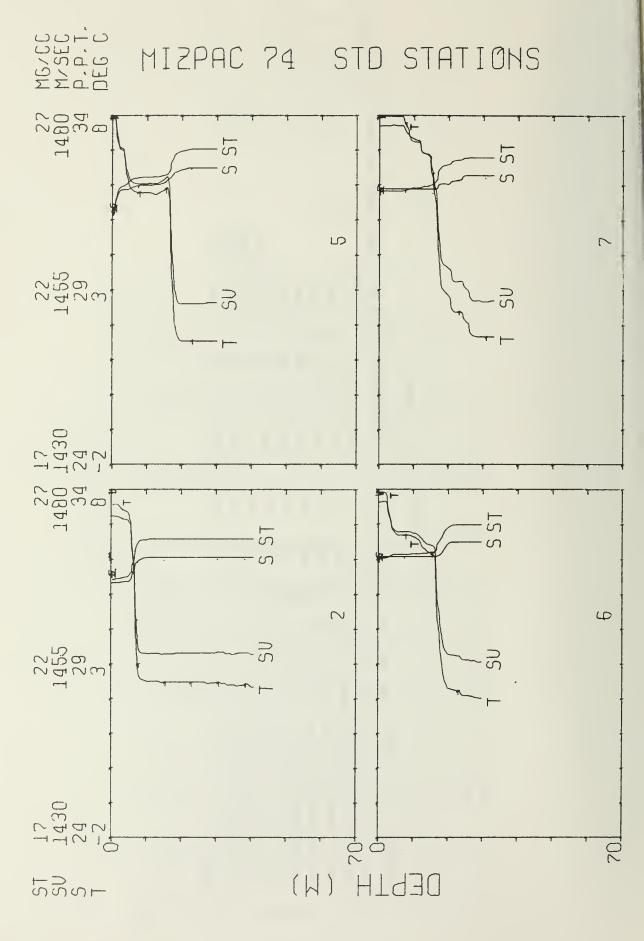
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088	443	143	130	463	438	104	092	420	448	070	060	235	320	141	138	382	380	3 80	960	485
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	13.9 0840	13.9 0848	15.1 0858	15.1 085D	16.6 086D	16.6 086	17.7 087	17.7 087	19.5 088	19.5 0888	23.6 089	23.6 089	00.5 090	060 5.00	02.7 0918	02.7 0910	04.3 0920	04.3 0925	06.4 0938	06 44 093
HR STA	13.9	74 13.9	15.1	15.1	16.6	16.6	17.7	17.7	19.5	19.5	23.6	23.6	9.00	00.5	02.7	02.7	04.3	04.3	4.90	06 °-4
HR STA	13.9	24 74 13.9	24 74 15.1	15.1	16.6	24 74 16.6	17.7	17.7	19.5	19.5	23.6	23.6	9.00	00.5	02.7	25 74 02.7	04.3	04.3	25 74 06.4	06 °-4
MD DY YR HR STA	07 24 74 13.9	07 24 74 13.9	07 24 74 15.1	07 24 74 15.1	07 24 74 16.6	07 24 74 16.6	07 24 74 17.7	07 24 74 17.7	07 24 74 19.5	07 24 74 19.5	07 24 74 23.6	07 24 74 23.6	07 25 74 00.5	07 25 74 00.5	07 25 74 02.7	07 25 74 02.7	07 25 74 04.3	07 25 74 04.3	07 25 74 06.4	07 25 74 06 4
HR STA	13.9	24 74 13.9	24 74 15.1	15.1	16.6	24 74 16.6	17.7	17.7	19.5	19.5	23.6	23.6	9.00	00.5	02.7	25 74 02.7	04.3	04.3	25 74 06.4	06 °-4
45Q MO DY YR HR STA	269 07 24 74 13.9	269 07 24 74 13.9	269 07 24 74 15.1	269 07 24 74 15.1	269 07 24 74 16.6	269 07 24 74 16.6	2'69 07 24 74 17.7	269 07 24 74 17.7	269 07 24 74 19.5	269 07 24 74 19.5	269 07 24 74 23.6	269 07 24 74 23.6	269 07 25 74 00.5	269 07 25 74 00.5	269 07 25 74 02.7	269 07 25 74 02.7	269 07 25 74 04.3	269 07 25 74 04.3	269 07 25 74 06.4	269 07 25 74 06 4
MD DY YR HR STA	269 07 24 74 13.9	269 07 24 74 13.9	269 07 24 74 15.1	269 07 24 74 15.1	269 07 24 74 16.6	269 07 24 74 16.6	2'69 07 24 74 17.7	269 07 24 74 17.7	269 07 24 74 19.5	269 07 24 74 19.5	269 07 24 74 23.6	269 07 24 74 23.6	269 07 25 74 00.5	269 07 25 74 00.5	269 07 25 74 02.7	269 07 25 74 02.7	269 07 25 74 04.3	269 07 25 74 04.3	269 07 25 74 06.4	269 07 25 74 06 4
45Q MO DY YR HR STA	164-02.0 269 07 24 74 13.9	164-02.0 269 07 24 74 13.9	163-55.0 269 07 24 74 15.1	163-55.0 269 07 24 74 15.1	163-45.0 269 07 24 74 16.6	163-45.0 269 07 24 74 16.6	163-33.0 2'69 07 24 74 17.7	163-33.0 269 07 24 74 17.7	163-11.1 269 07 24 74 19.5	163-11.1 269 07 24 74 19.5	163-01.3 269 07 24 74 23.6	163-01.3 269 07 24 74 23.6	163-12.5 269 07 25 74 00.5	163-12.5 269 07 25 74 00.5	163-24.0 269 07 25 74 02.7	163-24.0 269 07 25 74 02.7	163-34.8 269 07 25 74 04.3	163-34.8 269 07 25 74 04.3	163-44.5 269 07 25 74 06.4	163-44.5 269 07 25 74 06.4
LCNG 45Q MD DY YR HR STA	164-02.0 269 07 24 74 13.9	164-02.0 269 07 24 74 13.9	163-55.0 269 07 24 74 15.1	163-55.0 269 07 24 74 15.1	163-45.0 269 07 24 74 16.6	163-45.0 269 07 24 74 16.6	163-33.0 2'69 07 24 74 17.7	163-33.0 269 07 24 74 17.7	163-11.1 269 07 24 74 19.5	163-11.1 269 07 24 74 19.5	163-01.3 269 07 24 74 23.6	163-01.3 269 07 24 74 23.6	163-12.5 269 07 25 74 00.5	163-12.5 269 07 25 74 00.5	163-24.0 269 07 25 74 02.7	163-24.0 269 07 25 74 02.7	163-34.8 269 07 25 74 04.3	163-34.8 269 07 25 74 04.3	163-44.5 269 07 25 74 06.4	163-44.5 269 07 25 74 06.4
LCNG 45Q MD DY YR HR STA	164-02.0 269 07 24 74 13.9	164-02.0 269 07 24 74 13.9	70-09.8 163-55.0 269 07 24 74 15.1	70-09.8 163-55.0 269 07 24 74 15.1	163-45.0 269 07 24 74 16.6	163-45.0 269 07 24 74 16.6	70-17.8 163-33.0 269 07 24 74 17.7	163-33.0 269 07 24 74 17.7	70-25.3 163-11.1 269 07 24 74 19.5	70-25.3 163-11.1 269 07 24 74 19.5	70-06.4 163-01.3 269 07 24 74 23.6	163-01.3 269 07 24 74 23.6	70-10.0 163-12.5 269 07 25 74 00.5	70-10.0 163-12.5 269 07 25 74 00.5	163-24.0 269 07 25 74 02.7	70-12.9 163-24.0 269 07 25 74 02.7	70-15.8 163-34.8 269 07 25 74 04.3	70-15.8 163-34.8 269 07 25 74 04.3	70-20.0 163-44.5 269 07 25 74 06.4	163-44.5 269 07 25 74 06.4
LCNG 45Q MD DY YR HR STA	269 07 24 74 13.9	269 07 24 74 13.9	163-55.0 269 07 24 74 15.1	163-55.0 269 07 24 74 15.1	269 07 24 74 16.6	269 07 24 74 16.6	163-33.0 2'69 07 24 74 17.7	269 07 24 74 17.7	163-11.1 269 07 24 74 19.5	163-11.1 269 07 24 74 19.5	163-01.3 269 07 24 74 23.6	269 07 24 74 23.6	163-12.5 269 07 25 74 00.5	163-12.5 269 07 25 74 00.5	269 07 25 74 02.7	163-24.0 269 07 25 74 02.7	163-34.8 269 07 25 74 04.3	163-34.8 269 07 25 74 04.3	BI 70-20.0 163-44.5 269 07 25 74 06.4	81 70-20.0 163-44.5 269 07 25 74 06.4
45Q MO DY YR HR STA	164-02.0 269 07 24 74 13.9	164-02.0 269 07 24 74 13.9	70-09.8 163-55.0 269 07 24 74 15.1	70-09.8 163-55.0 269 07 24 74 15.1	163-45.0 269 07 24 74 16.6	163-45.0 269 07 24 74 16.6	70-17.8 163-33.0 269 07 24 74 17.7	163-33.0 269 07 24 74 17.7	70-25.3 163-11.1 269 07 24 74 19.5	70-25.3 163-11.1 269 07 24 74 19.5	70-06.4 163-01.3 269 07 24 74 23.6	163-01.3 269 07 24 74 23.6	70-10.0 163-12.5 269 07 25 74 00.5	70-10.0 163-12.5 269 07 25 74 00.5	163-24.0 269 07 25 74 02.7	70-12.9 163-24.0 269 07 25 74 02.7	70-15.8 163-34.8 269 07 25 74 04.3	70-15.8 163-34.8 269 07 25 74 04.3	70-20.0 163-44.5 269 07 25 74 06.4	163-44.5 269 07 25 74 06.4

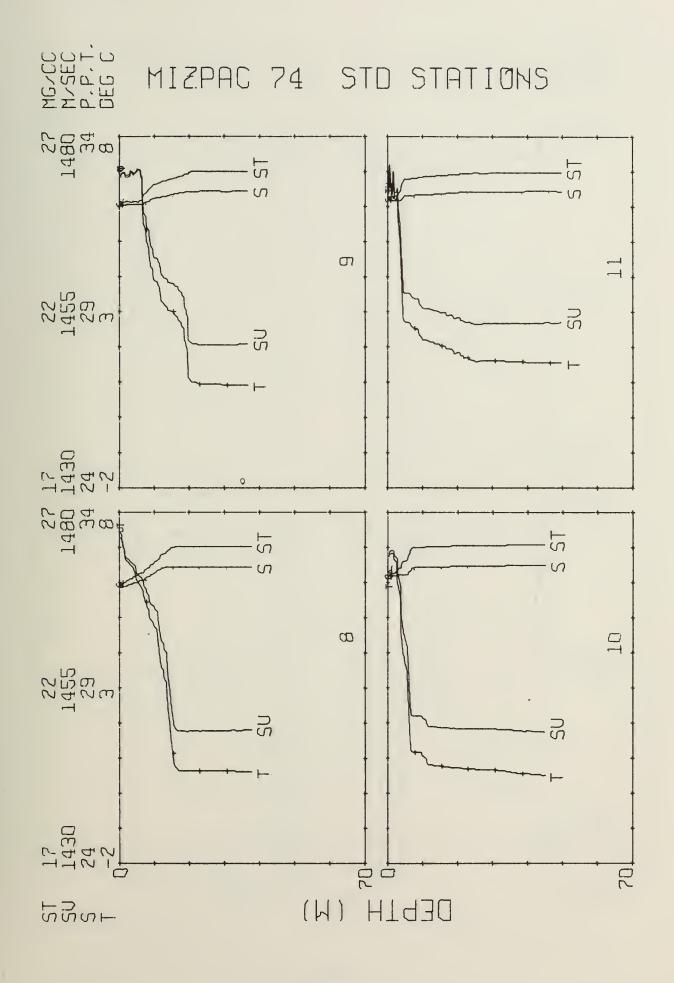
MIZPAC 74 STD STATIONS

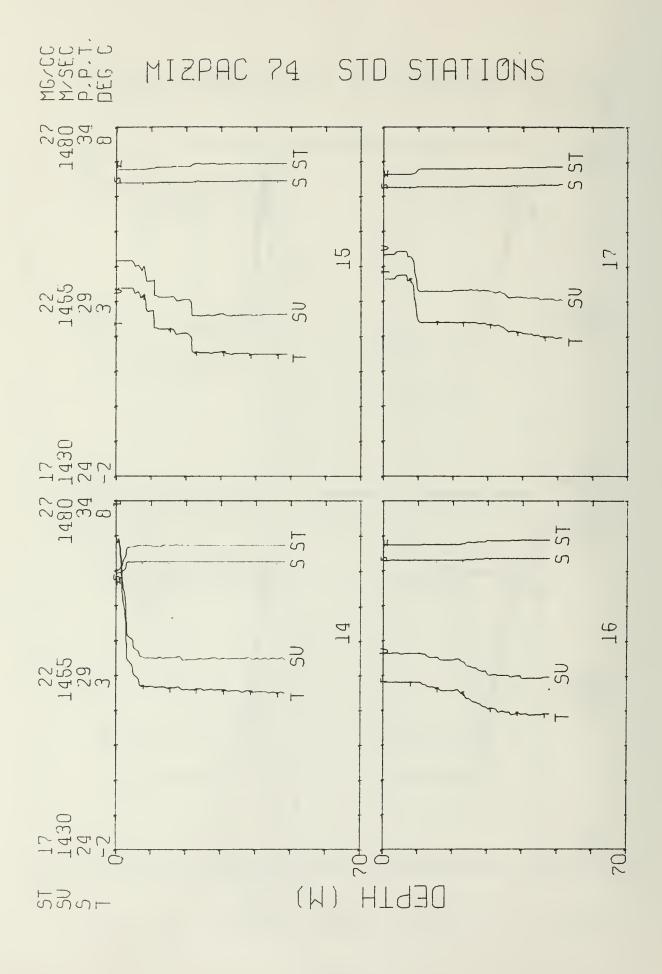
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	LCNG	153-48.7	163-48.7	163-50.0	163-50.0	163-30.0	163-30.9	163-12.5	163-12.5	162-49.6	162-49.8	162-39.7	162-39.7	162-31.4	162-31.4	163-56.1	163-56.3	163-56.3	163-47.5	165-01.3	165-04.0
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	LAT	70-23	70-23	70-29	70-29	70-33	70-4	70-4	70-4	70-3	70-3	70-3	70-3	70-3	70-3	70-2	7 0-3	70-3	20-3	70-26	70-2
	HIP LAT	81 70-23.8	BI 70-23.8	BI 70-29.4	81 70-29.4	BI 70-33.6	BI 70-43.4	BI 70-41.0	81 70-41.0	BI 70-37.0	BI 70-37.0	BI 70-37.3	BI 70-37.3	BI 70-37.7	BI 70-37.7	81 70-25.1	BI 70-36.6	BI 70-36.6	BI 70-37.6	BI 70-26.3	BI 70-2
	NAT SHIP LAT	31 81 70-23.	31 BI 70-23					31 81 70-4	31 81 70-4	31 81 70-3	31 81 70-3	31 81 70-3	31 BI 70-3	31 BI 70-3	31 81 70-3	31 81 70-2	31 81 70-3	31 BI 70-3	31 81 70-3	31 BI 70-20	31 BI 70-26.5

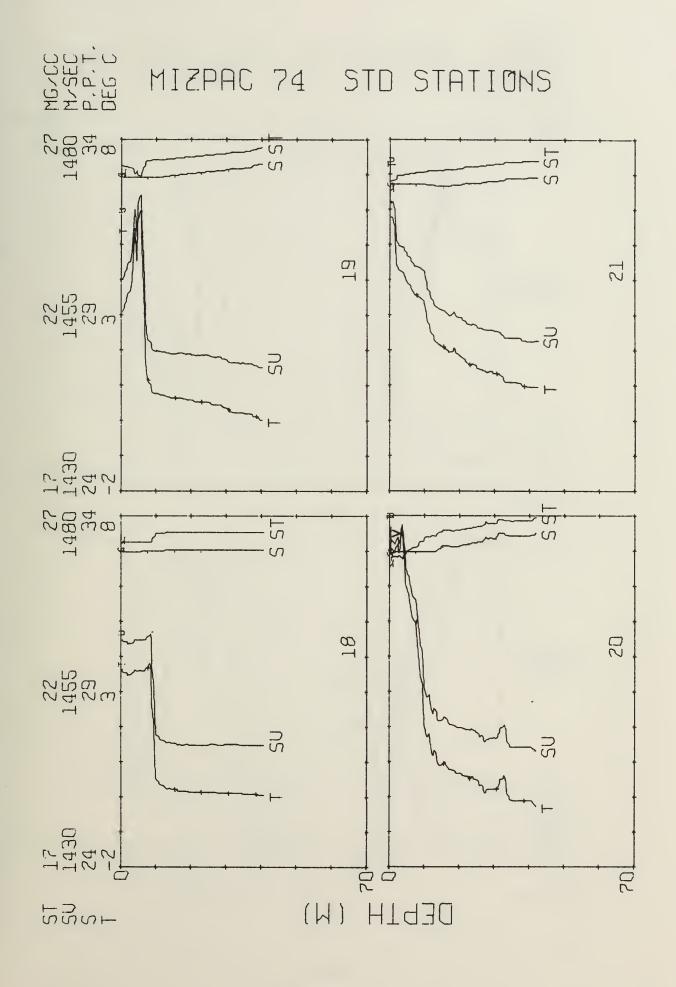
MIZPAC 74 STD STATIONS

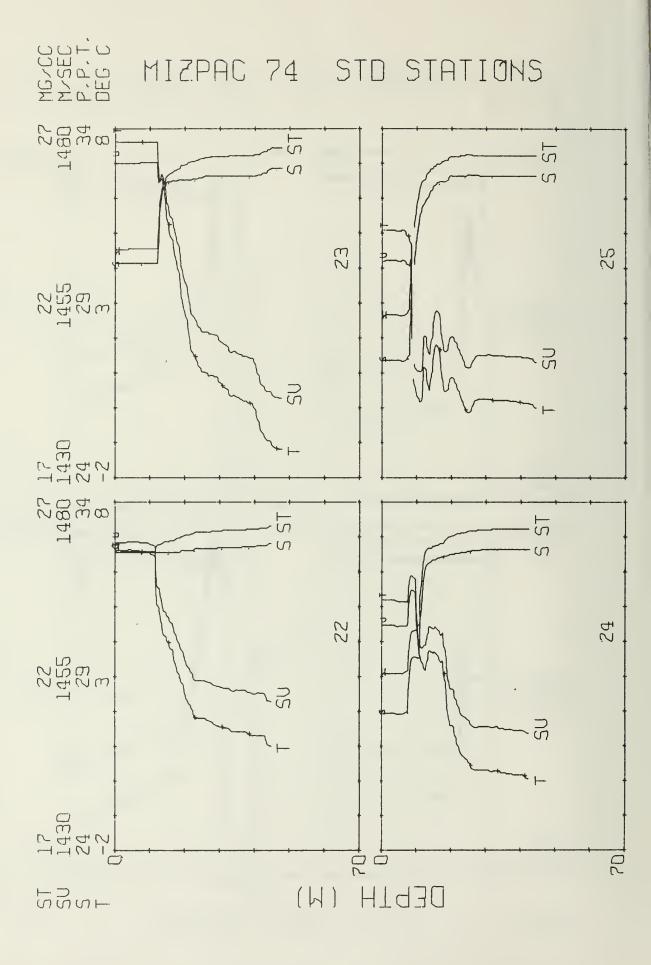
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DRY										
BAR						010	010	010	010	
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PER	×	×	×	×	×	×	×	×	×	
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HR STA	16.0 107	17.4 1080	17.4 1085	18.5 1095	18.5 1090	19.5 1100	19.5 1105	20.2 1115	20.2 1110	
HR STA	16.0 107	17.4 1080	17.4 1085	18.5 1095	18.5 1090	19.5 1100	19.5 1105	20.2 1115	20.2 1110	
HR STA	16.0 107	17.4 1080	17.4 1085	18.5 1095	18.5 1090	19.5 1100	19.5 1105	20.2 1115	20.2 1110	
HR STA	16.0 107	07 26 74 17.4 108D	07 26 74 17.4 1085	07 26 74 18.5 1095	18.5 1090	19.5 1100	07 26 74 19.5 1105	07 26 74 20.2 1115	07 26 74 20.2 1110	
MSQ MO DY YR HR STA	269 07 26 74 16.0 107	269 07 26 74 17.4 1080	269 07 26 74 17.4 1085	269 07 26 74 18.5 1095	269 07 26 74 18.5 1090	269 07 26 74 19.5 1100	269 07 26 74 19.5 1105	269 07 26 74 20.2 1115	07 26 74 20.2 1110	
MSQ MO DY YR HR STA	269 07 26 74 16.0 107	269 07 26 74 17.4 1080	269 07 26 74 17.4 1085	269 07 26 74 18.5 1095	269 07 26 74 18.5 1090	269 07 26 74 19.5 1100	269 07 26 74 19.5 1105	269 07 26 74 20.2 1115	07 26 74 20.2 1110	
HR STA	269 07 26 74 16.0 107	269 07 26 74 17.4 1080	269 07 26 74 17.4 1085	269 07 26 74 18.5 1095	269 07 26 74 18.5 1090	269 07 26 74 19.5 1100	269 07 26 74 19.5 1105	269 07 26 74 20.2 1115	07 26 74 20.2 1110	
LONG MSQ MO DY YR HR STA	269 07 26 74 16.0 107	269 07 26 74 17.4 1080	269 07 26 74 17.4 1085	269 07 26 74 18.5 1095	269 07 26 74 18.5 1090	269 07 26 74 19.5 1100	269 07 26 74 19.5 1105	269 07 26 74 20.2 1115	07 26 74 20.2 1110	
LONG MSQ MO DY YR HR STA	269 07 26 74 16.0 107	269 07 26 74 17.4 1080	269 07 26 74 17.4 1085	269 07 26 74 18.5 1095	269 07 26 74 18.5 1090	269 07 26 74 19.5 1100	269 07 26 74 19.5 1105	269 07 26 74 20.2 1115	07 26 74 20.2 1110	169
LONG MSQ MO DY YR HR STA	269 07 26 74 16.0 107	81 70-36.5 165-14.5 269 07 26 74 17.4 1080	BI 70-36.5 165-14.5 269 07 26 74 17.4 108S	81 70-40.0 165-14.6 269 07 26 74 18.5 1095	81 70-40.0 165-14.6 269 07 26 74 18.5 1090	81 70-43.9 165-17.0 269 07 26 74 19.5 1100	81 70-43.9 165-17.0 269 07 26 74 19.5 1105	BI 70-44.9 165-16.5 269 07 26 74 20.2 111S	81 70-44.9 165-16.5 269 07 26 74 20.2 1110	AL= 169
MSQ MO DY YR HR STA	16.0 107	269 07 26 74 17.4 1080	269 07 26 74 17.4 1085	269 07 26 74 18.5 1095	269 07 26 74 18.5 1090	269 07 26 74 19.5 1100	269 07 26 74 19.5 1105	269 07 26 74 20.2 1115	07 26 74 20.2 1110	T0TAL= 169

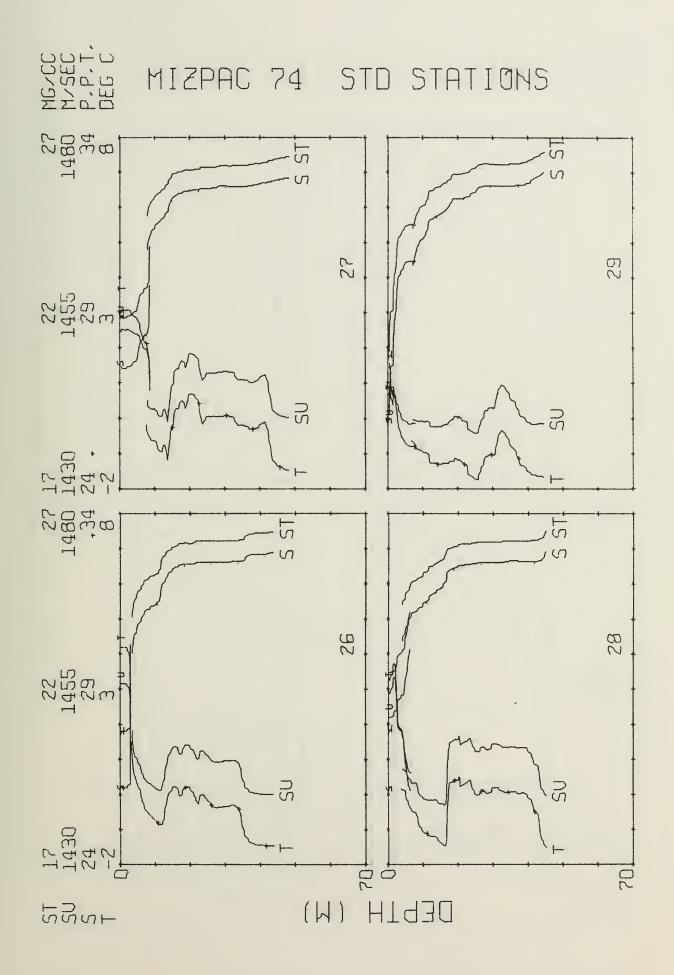


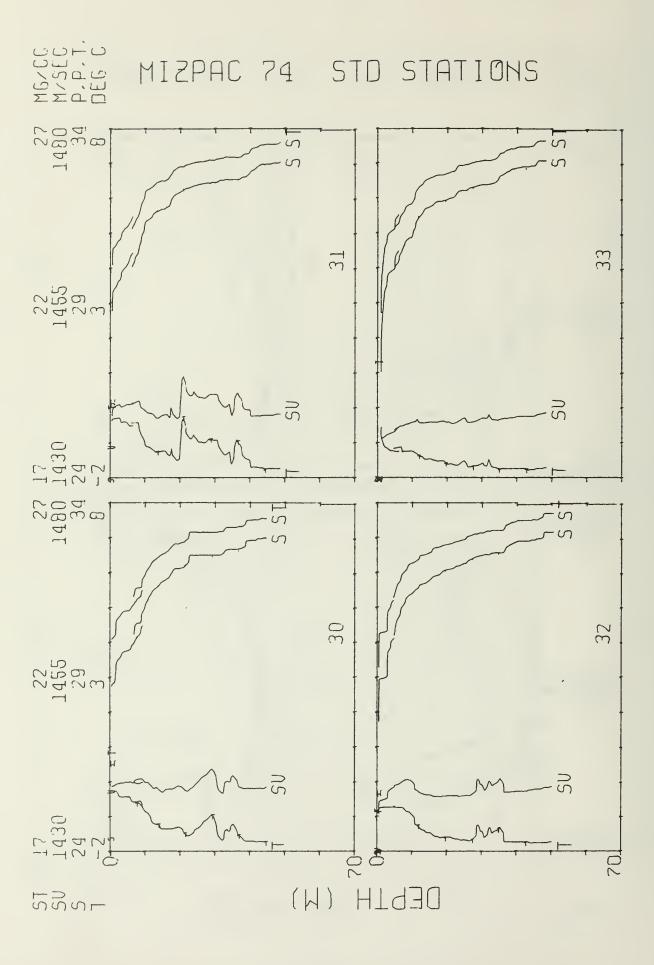


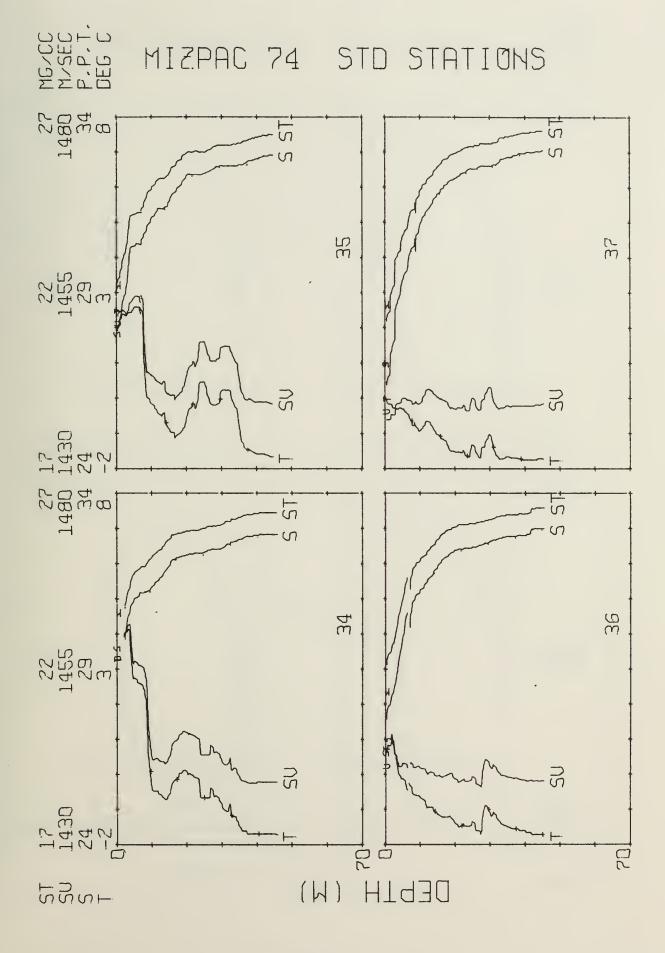


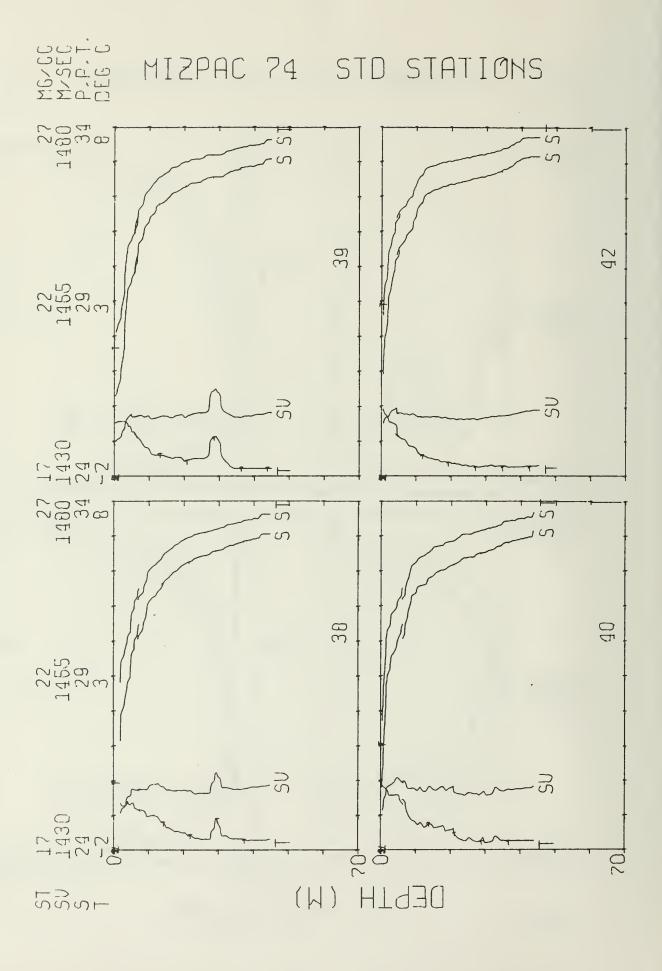


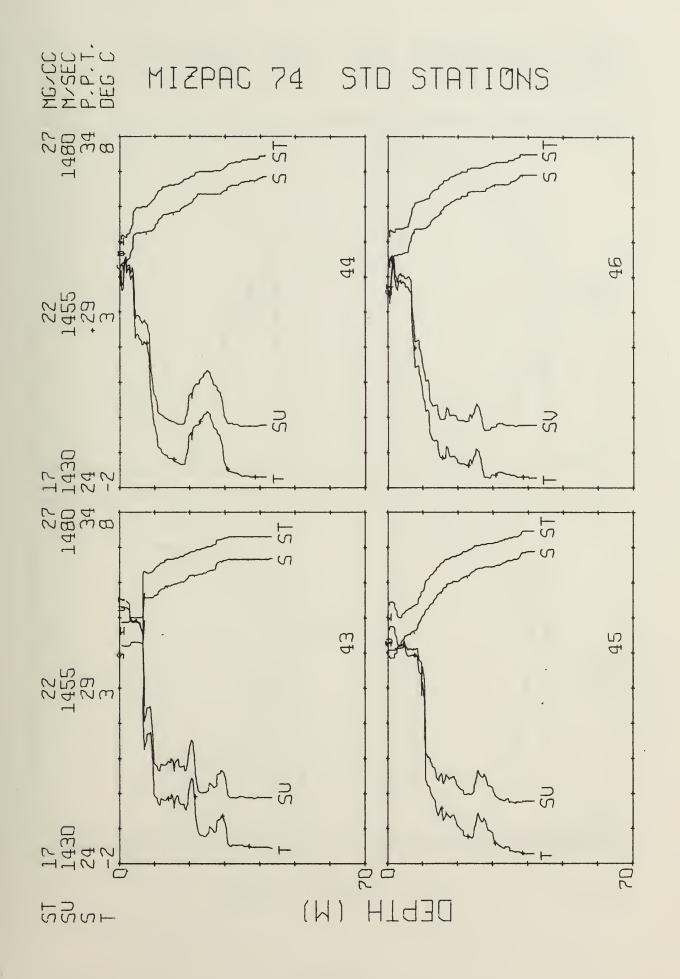


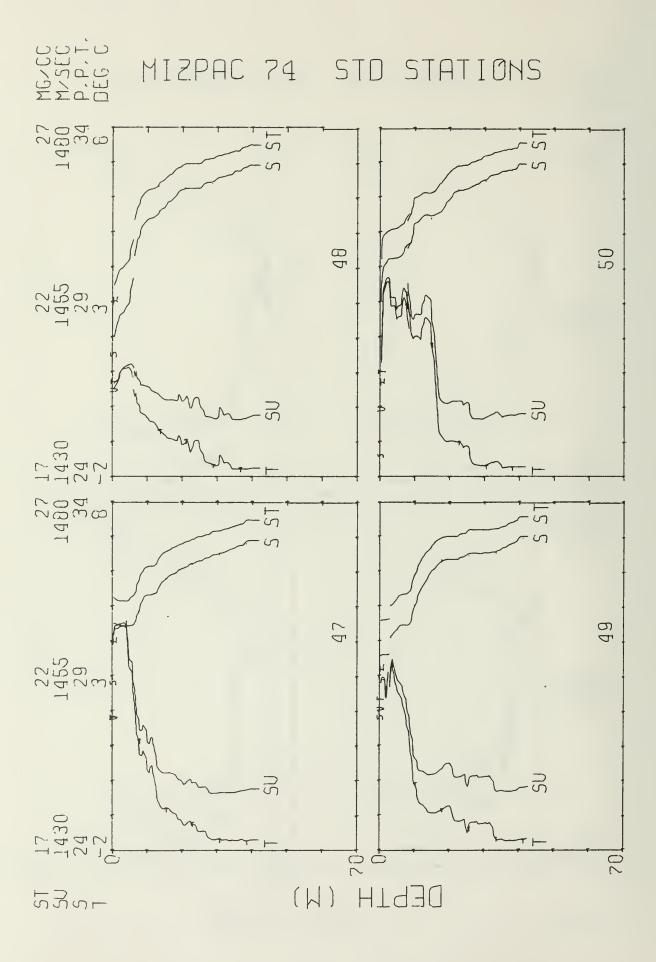


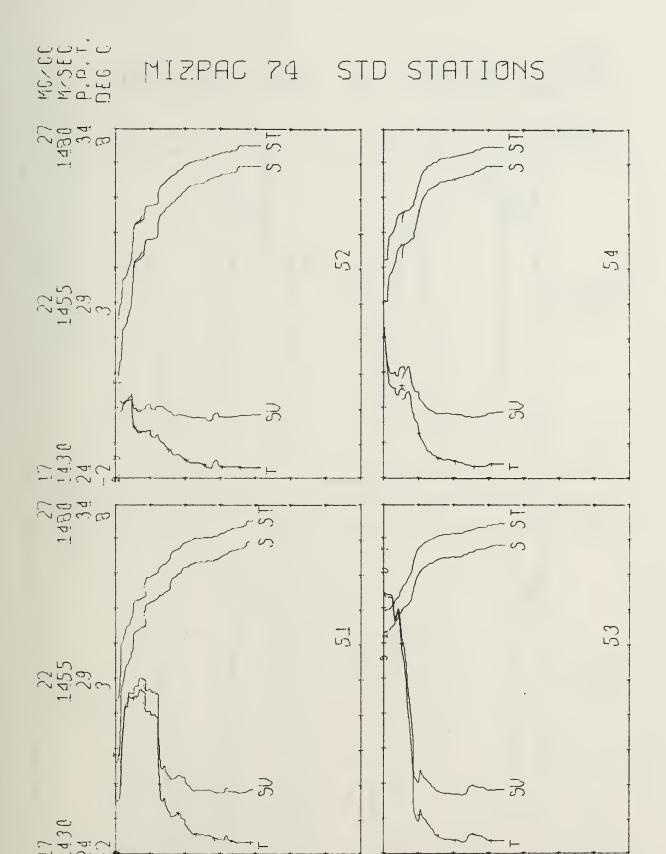






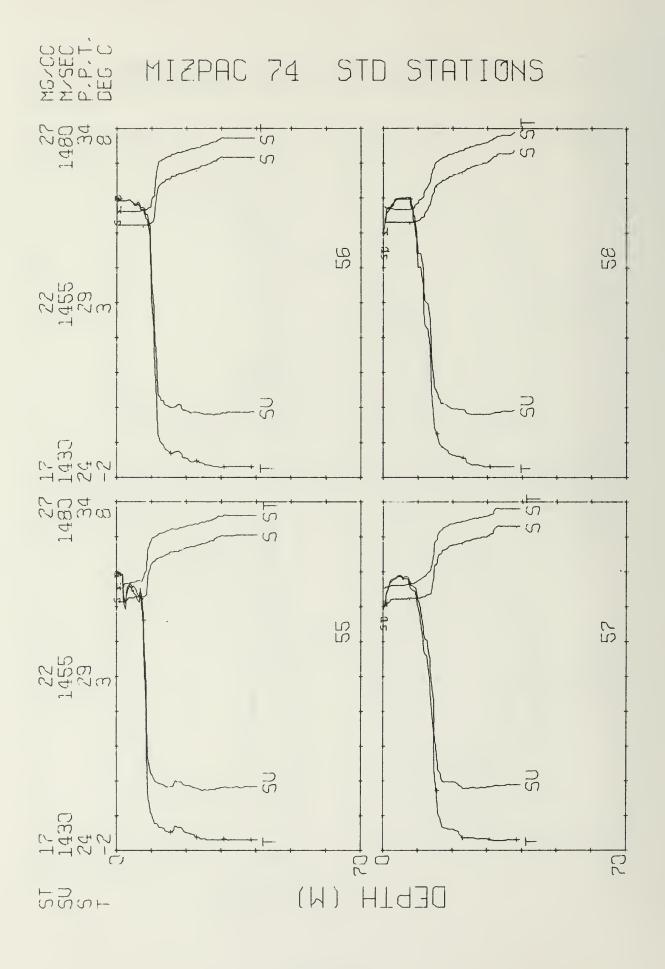


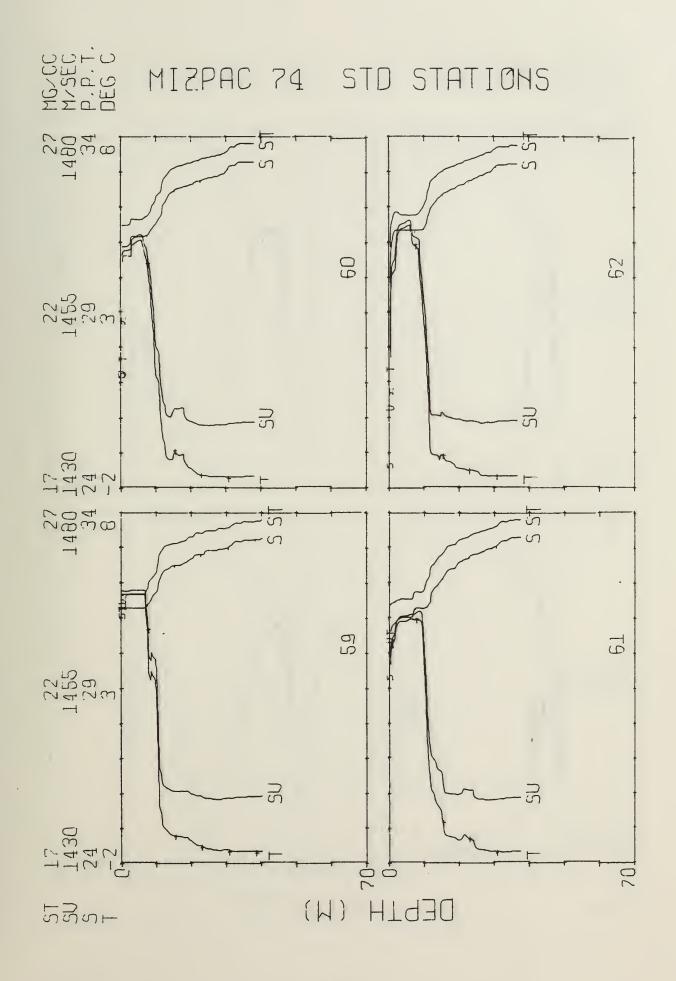


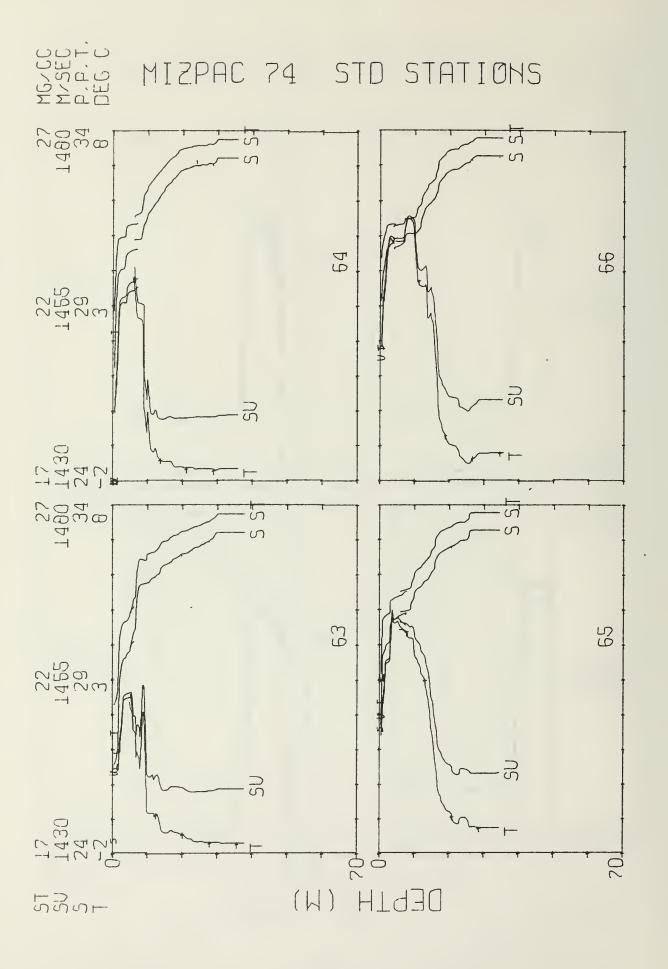


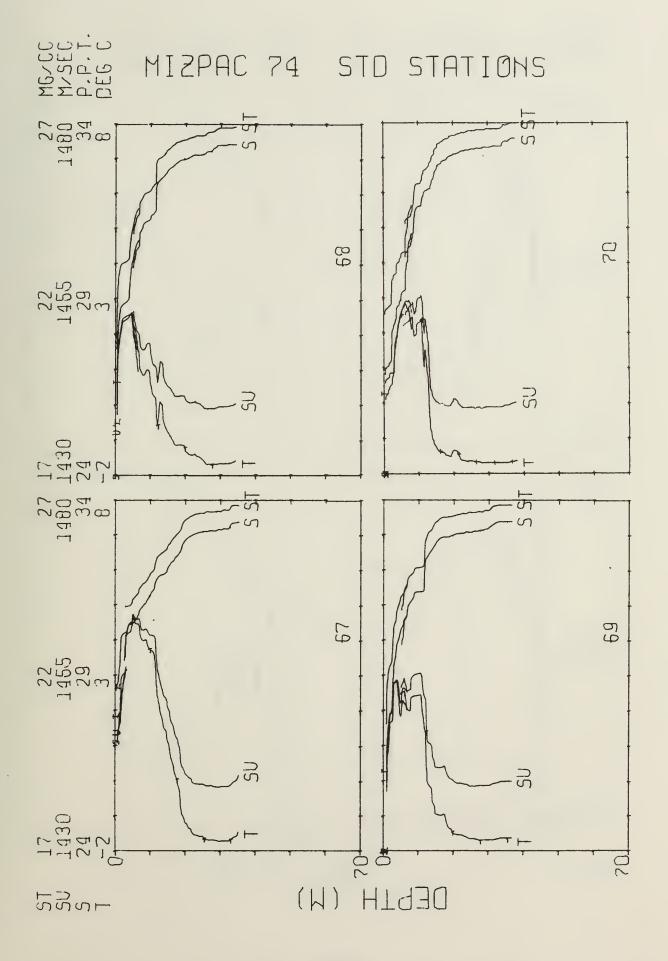
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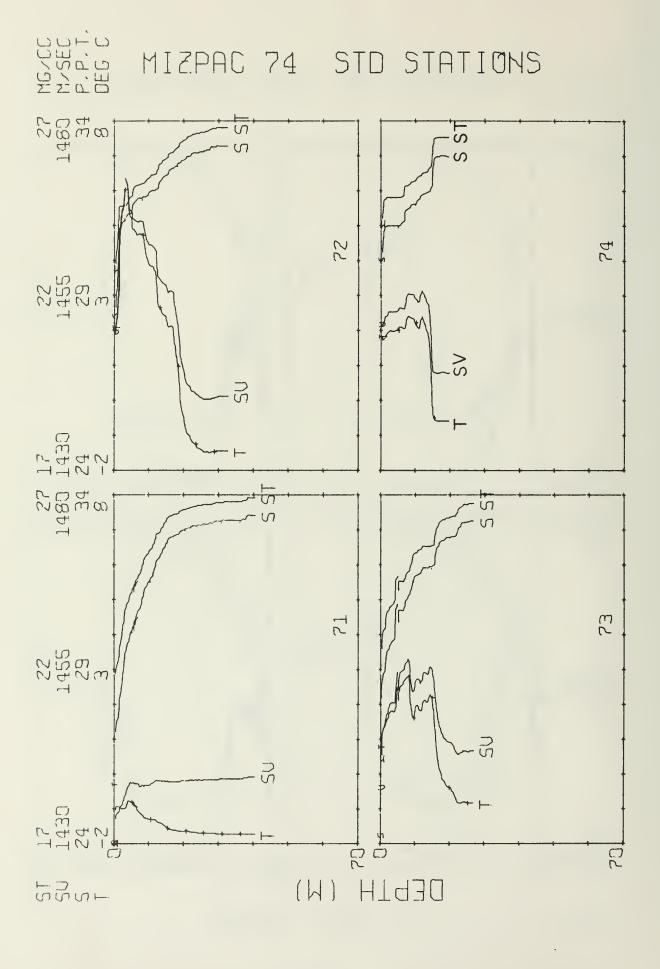
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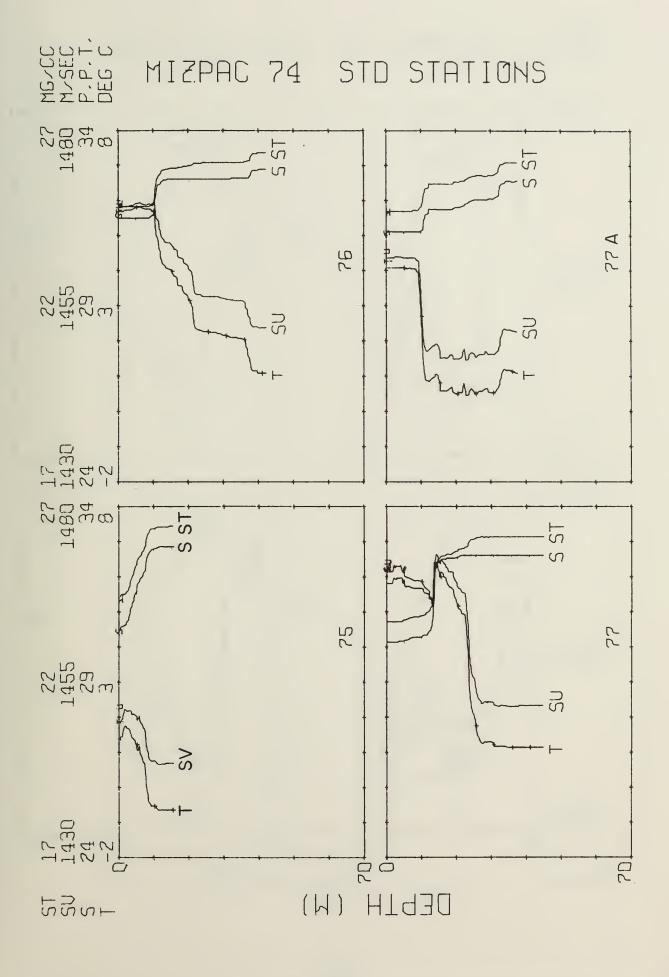


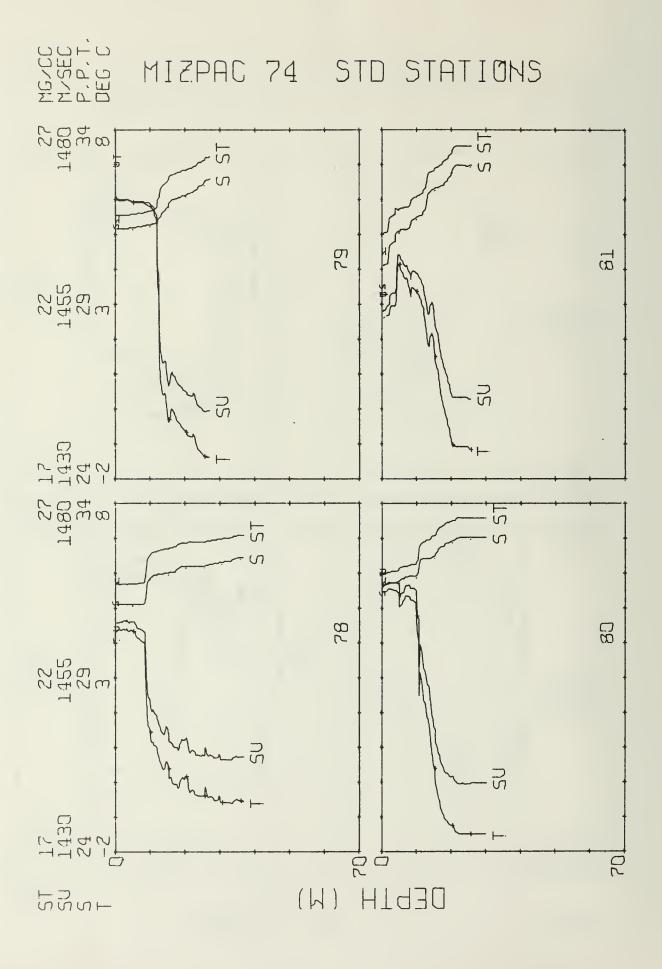


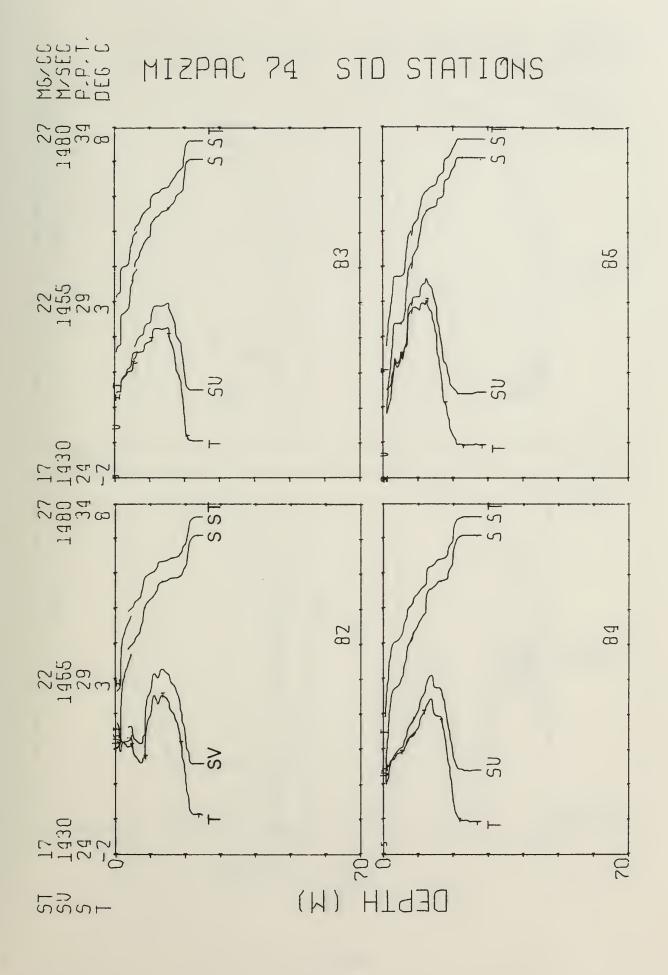


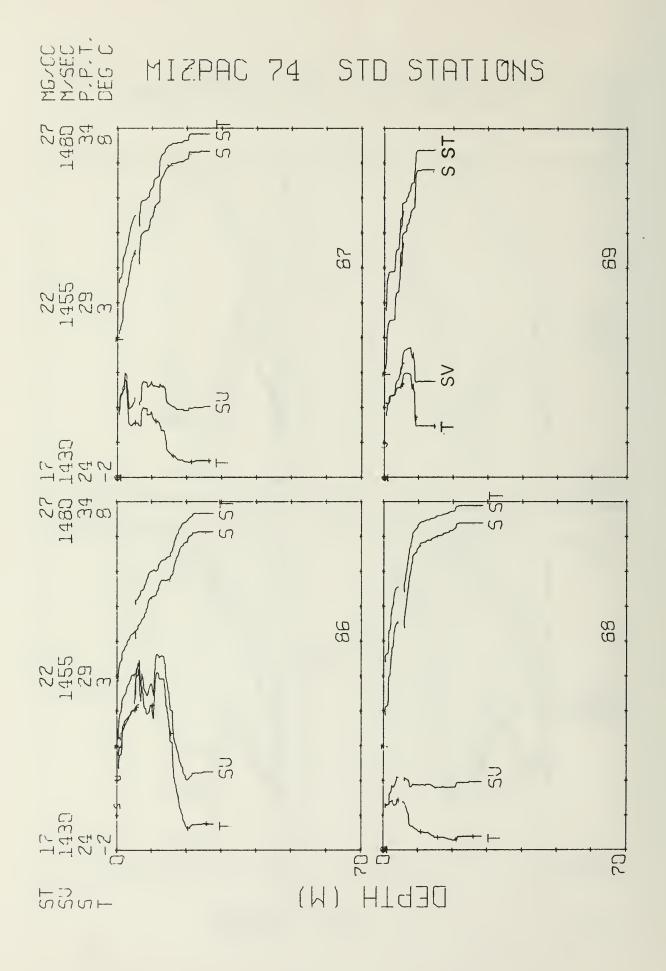


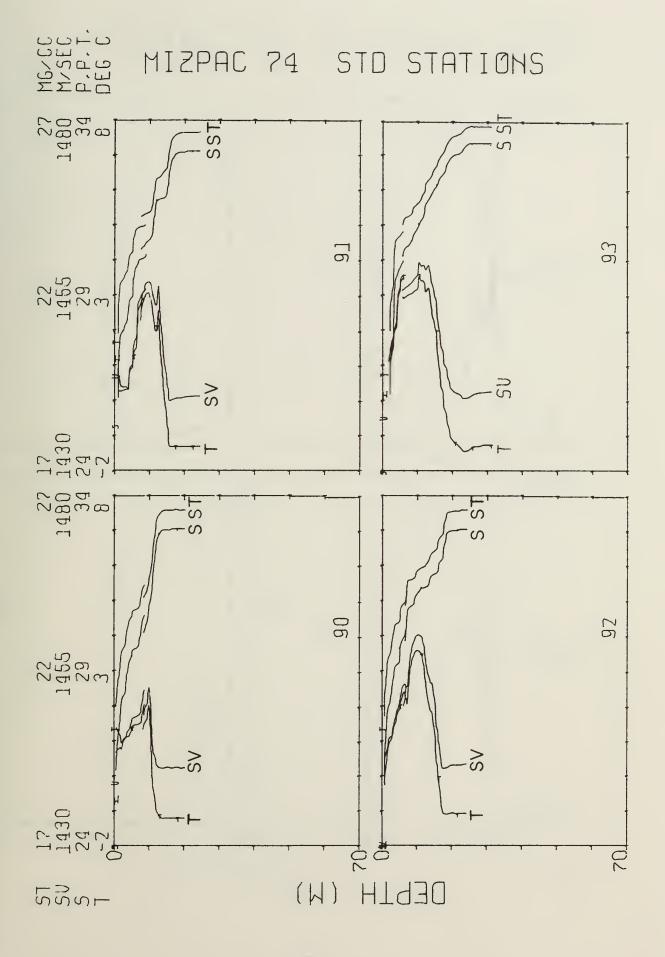


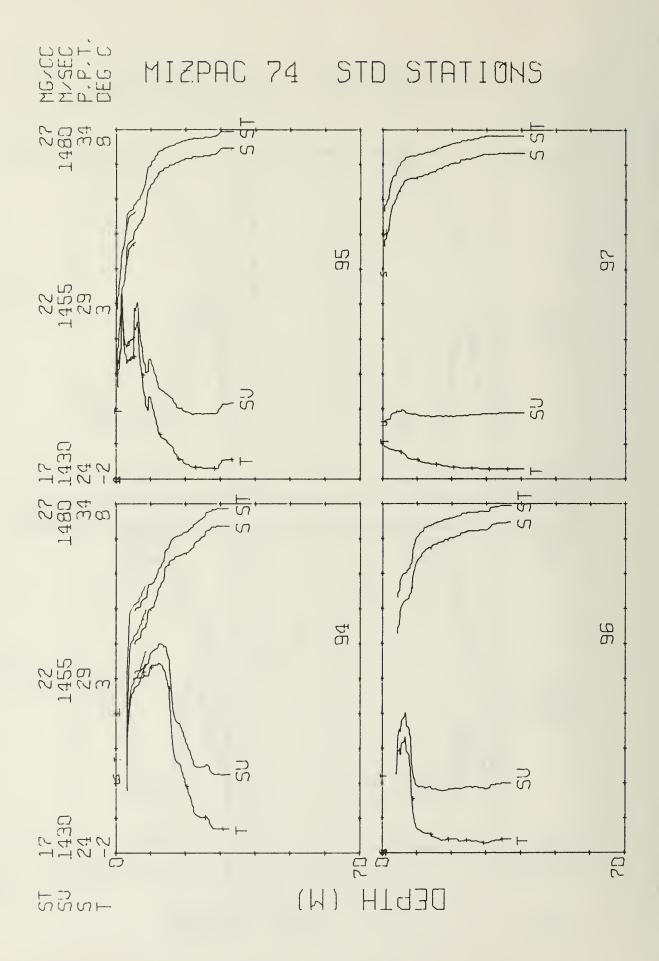


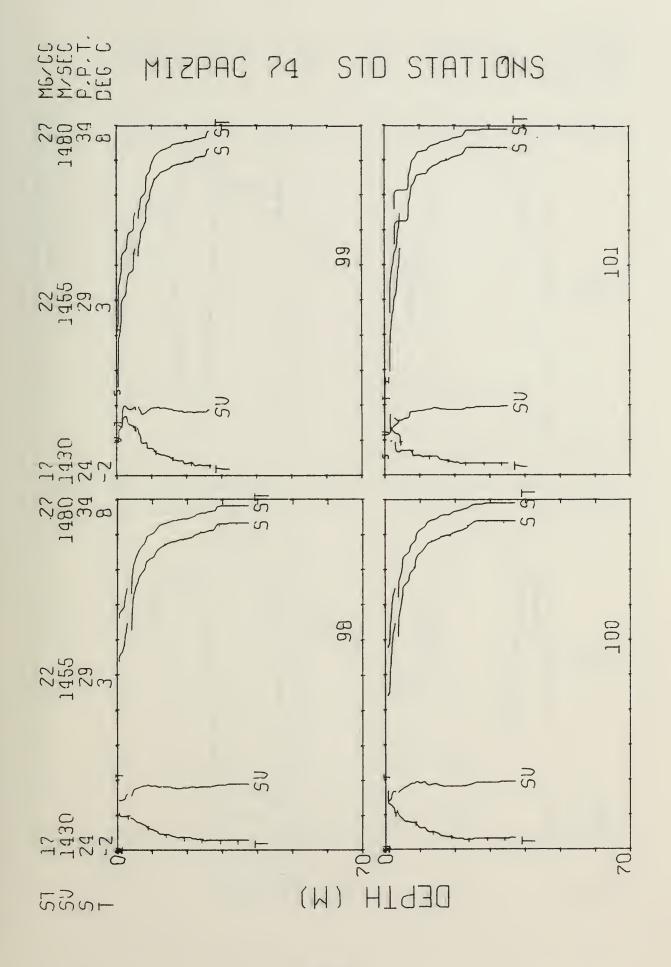


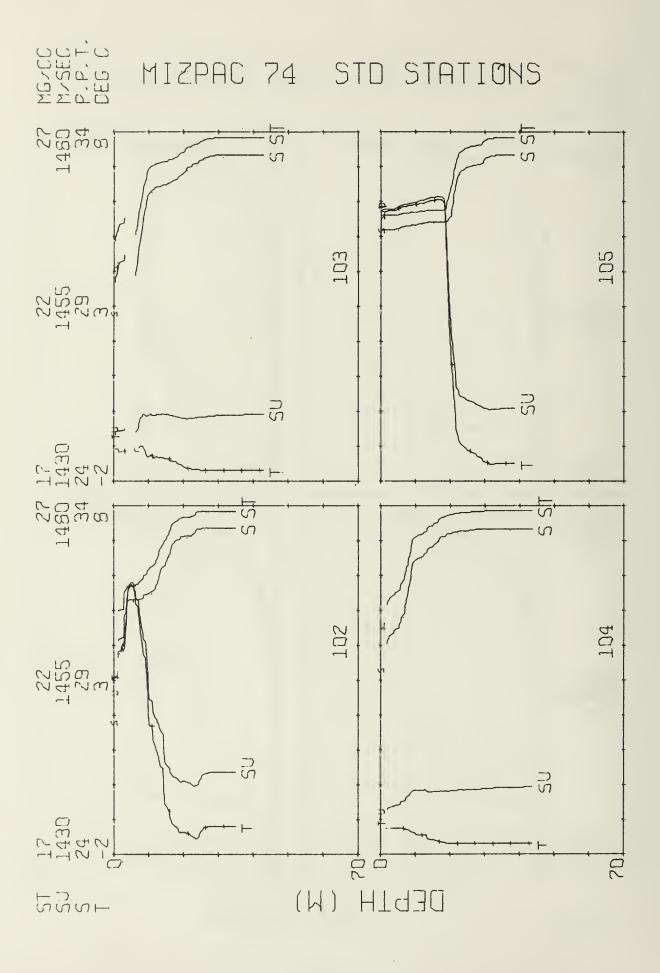


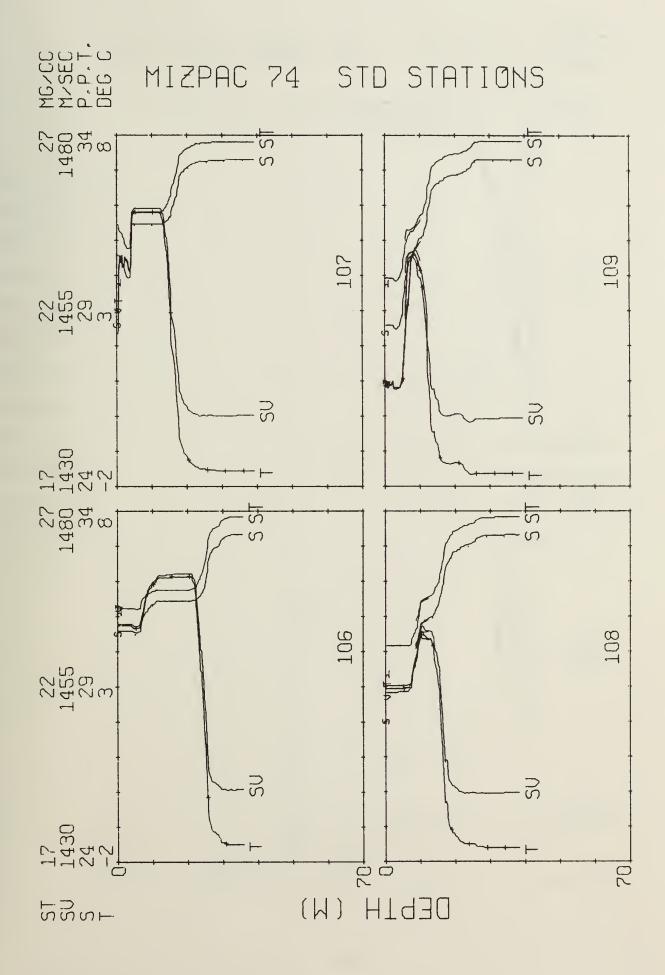


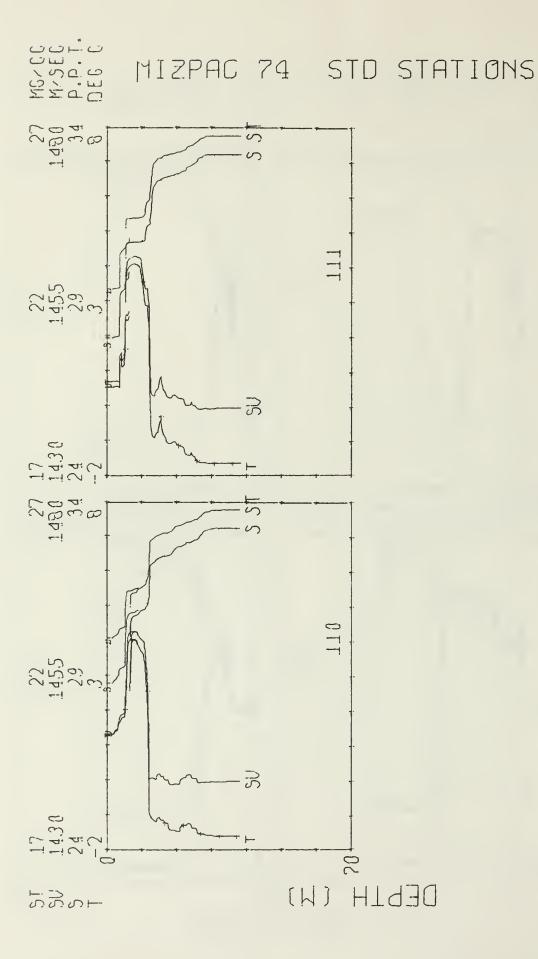












APPENDIX III

XBT HEADING DATA AND TEMPERATURE PROFILES

	Page
XBT Heading Data	III-1 to III-5
XBT Line 33	III-6
XBT Line 42	III-7
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XBT Line 64	III-10
XBT Line 71	III-11
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XBT Line 104	III-18, 19, 20
XBT Line 128	III-21, 22, 23, 24
XBT Line 138	III-25, 26

MIZPAC 74 X8T STATIONS

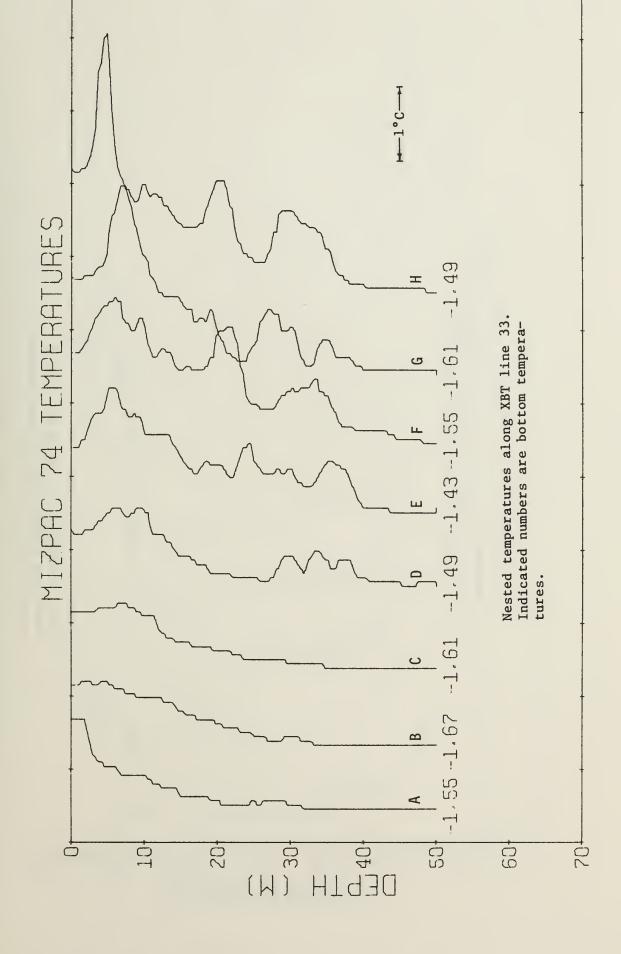
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NAT SHIP LAT	0.91-69	81 69-13.4	BI 69-12.1	BI 69-10.5	81 69-09.5	81 69-08.7	81 69-07.3	81 69-05.9	81 69-33.6	BI 69-32.0	BI 69-29.3	BI 69-28.0	81 69-26.0	81 69-23.7	BI 69-22.2	BI 69-20.9	81 69-32.0	81 69-28.8	81 69-28.7	81 69-27.3
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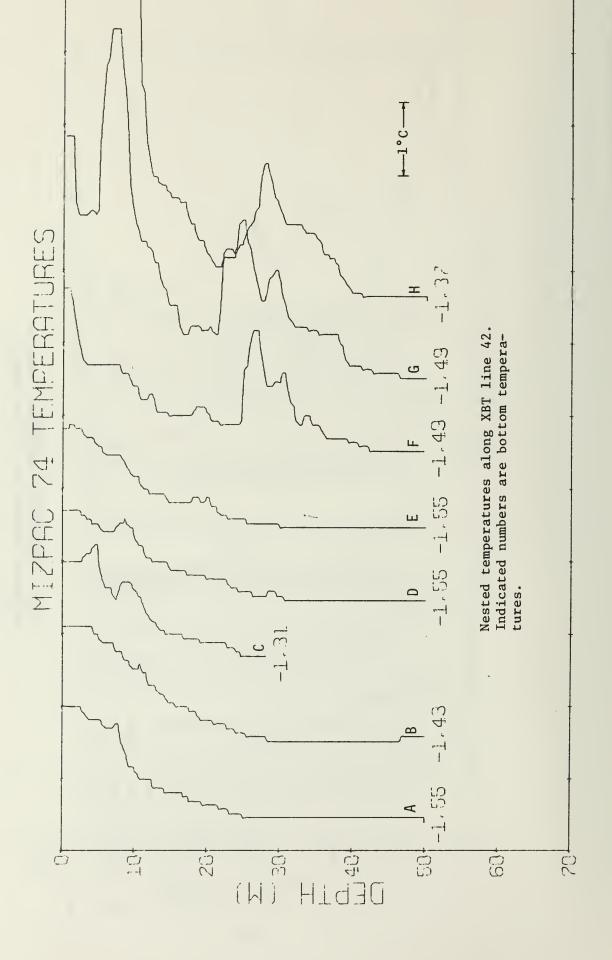
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STA	052F	03.0 0526	03.2 052H	03.4 0521	03.7 052J	04.0 052K	04.2 J52L		064A	071A	0718	0710	18.5 0710	071E	19.0 071F	0716	19.4 071H	0711	5 075A	09.7 075B
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LONG MSQ MO DY YR HR STA	167-36.4 233 07 20 74 02.8 052F	167-36.5 233 07 20 74 03.0 0526	167-37.0 233 07 20 74 03.2 052H	167-37.5 233 07 20 74 03.4 0521	167-38.0 233 07 20 74 03.7 0523	167-39.0 233 07 20 74 04.0 052K	167-39.0 233 07 20 74 04.2 352L	167-38.9 233 07 20 74 04.5	165-00.0 269 07 21 74 07.7 064A	164-21.0 269 07 21 74 17.3 071A	164-21.5 269 07 21 74 17.7 0718	164-22.2 269 07 21 74 18.1 071C	164-23.0 269 07 21 74 18.5 0710	164-23.8 269 07 21 74 18.7 071E	164-24.2 269 07 21 74 19.0 071F	164-24.6 269 07 21 74 19.2 0716	164-25.0 269 07 21 74 19.4 071H	164-25.5 269 07 21 74 19.7 07111	166-42.5 233 07 22 74 09.5 075A	09.7 075B
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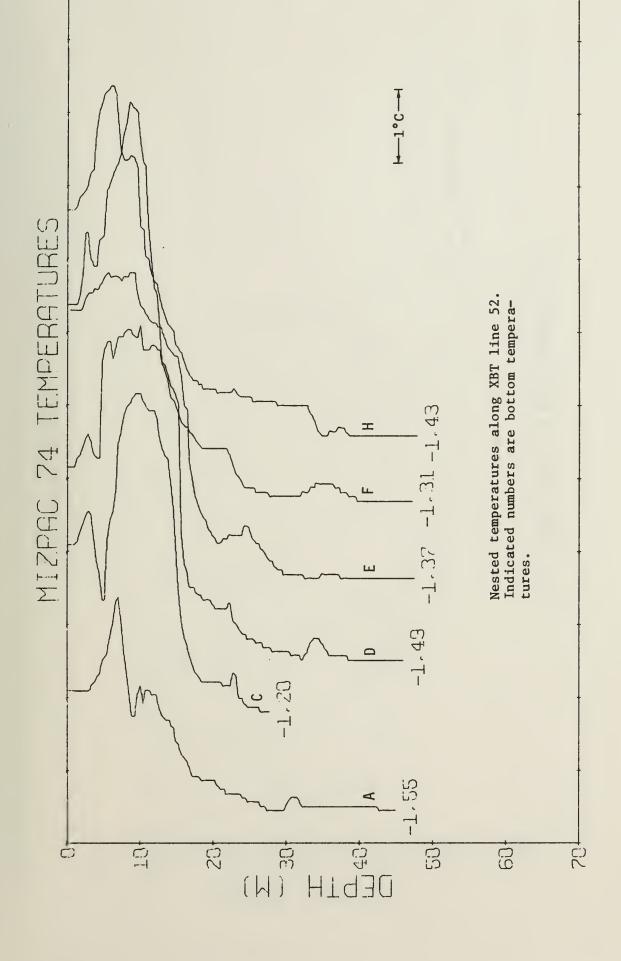
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H K	10.0	10.3	10.5	10.7	11.0	20.2	19.3	19.7	20.5	20.9	21.3	21.9	22.6	23.0	23.5	00.2	00.5	01.0	01.5	05.0
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LONG	167-00.5	167-09.5	167-18.5	167-27.5	167-35.5	165-57.0	163-01.0	163-10.0	163-19.5	70-19.5 163-23.5	163-28.2	163-31.8	163-39.3	163-45.0	163-51.5	164-00.0	164-03.0	184-05.0	164-03.2	164-02.0
NAT SHIP LAT	BI 68-57.0	BI 67-48.0	BI 70-30.0	70-26.0	81 70-21.5	70-19.5	BI 70-17.4	70-15.B	BI 70-11.7	70-08.5	BI 70-05.0	BI 70-01.0	BI 70-05.4	BI 70-09.6	81 70-14.2	BI 70-19.B				
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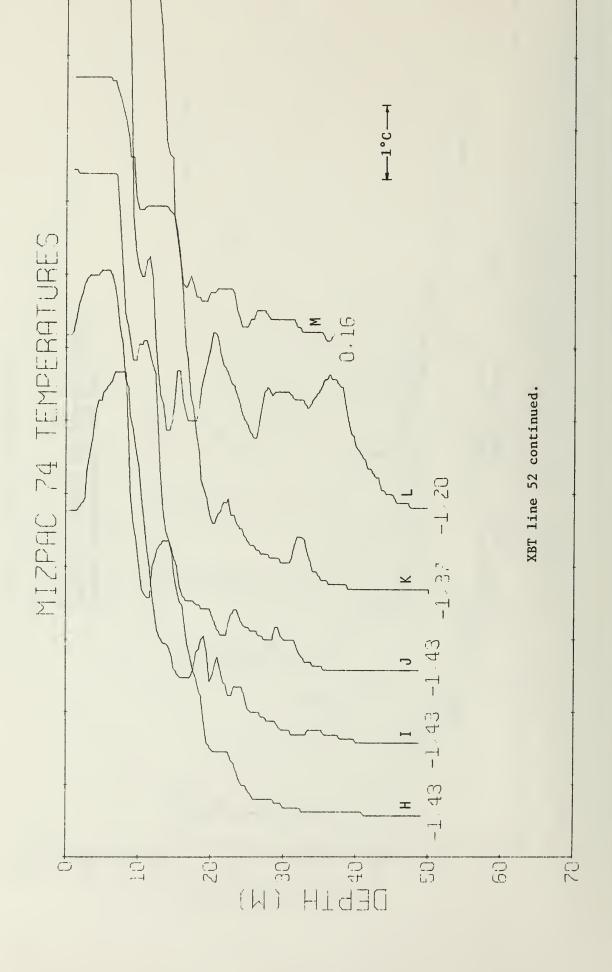
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	07.4 104A	08.4 1048	09.4 104C	10.4 104D	11.4 104E	12.0 104F	12.5 1046	13.0 104H	13.5 1041	17.8 128A	18.4 1288	18.9 1280	19.3 128D	19.8 128E	20.3 128F	20.8 1286	21.3 128Н	21.9 1281	22.4 128J	22.9 128
HR STA	4.70	08.4	4.60	10.4	11.4	12.0	12.5	13.0	13.5	17.8	18.4	18.9	19,3	19.8	20.3	20.8	21.3	21.9	22.4	22.9
HR STA	4.70	08.4	4.60	10.4	11.4	26 74 12.0	12.5	13.0	13.5	17.8	18.4	18.9	19,3	19.8	20.3	20.8	21.3	21.9	22.4	22.9
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MO DY YR HR STA	07 26 74 07.4	07 26 74 08.4	07 26 74 09.4	07 26 74 10.4	0.7 26 74 11.4	07 26 74 12.0	07 26 74 12.5	07 26 74 13.0	07 26 74 13.5	07 28 74 17.8	07 28 74 18.4	07 28 74 18.9	07 28 74 19.3	07 28 74 19.8	07 28 74 20.3	07 28 74 20.8	07 28 74 21.3	07 28 74 21.9	269 OJ 28 74 22.4	269 0.7 28 74 22.9
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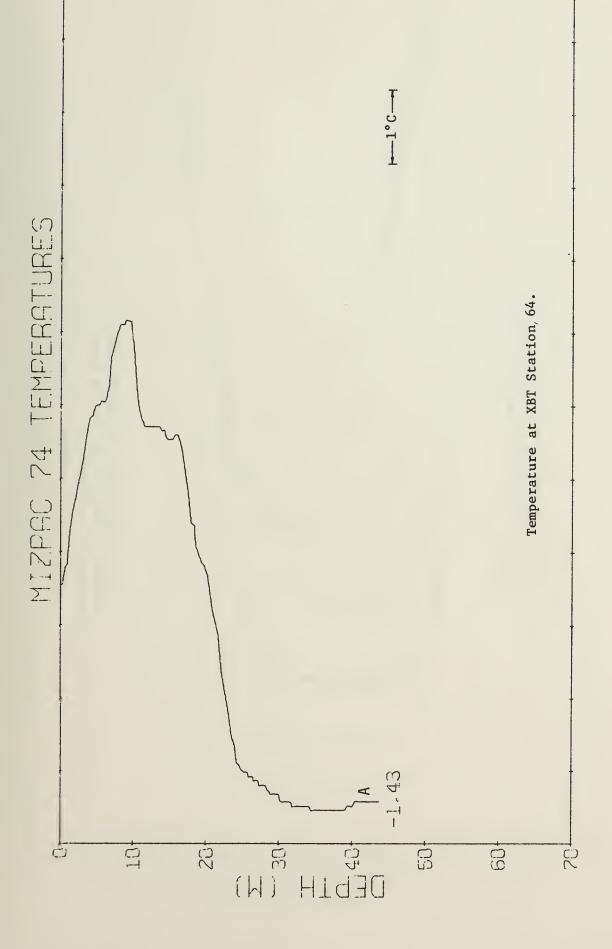
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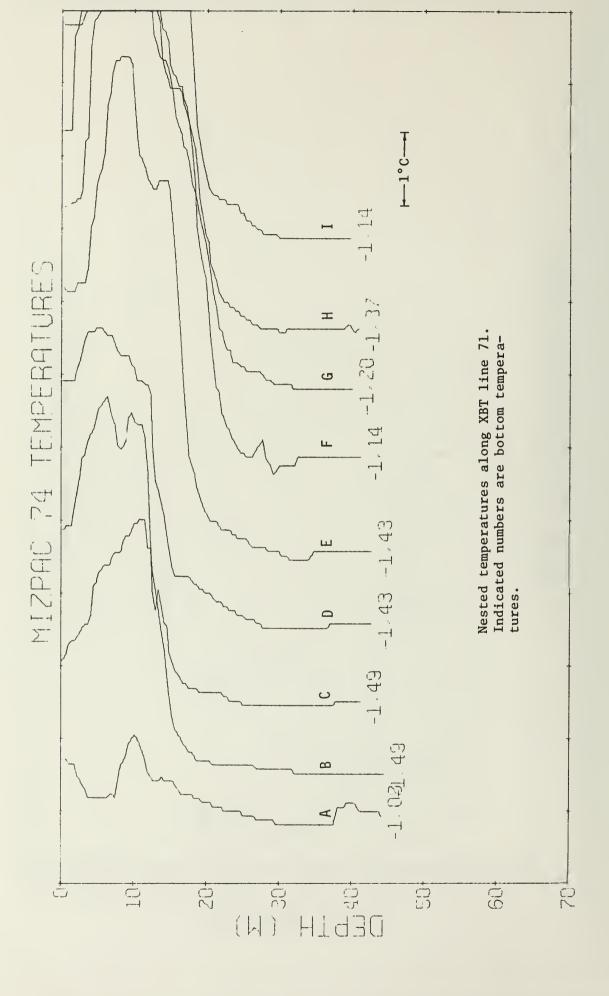


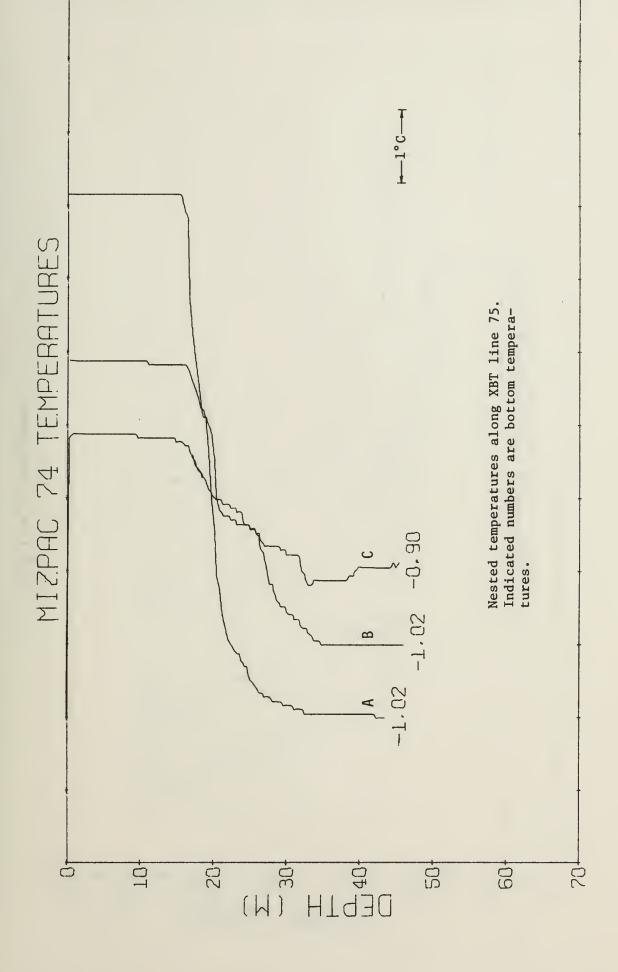


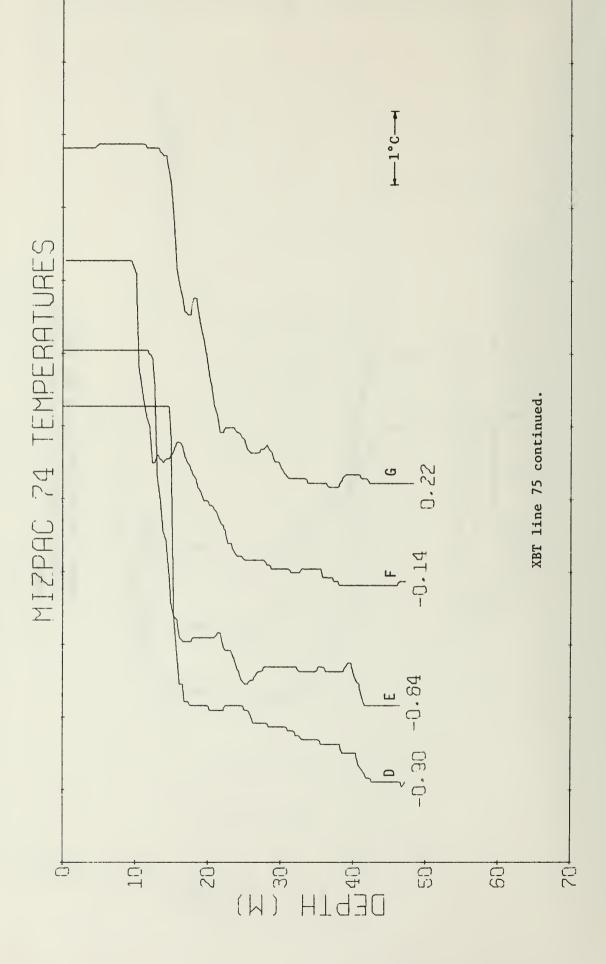


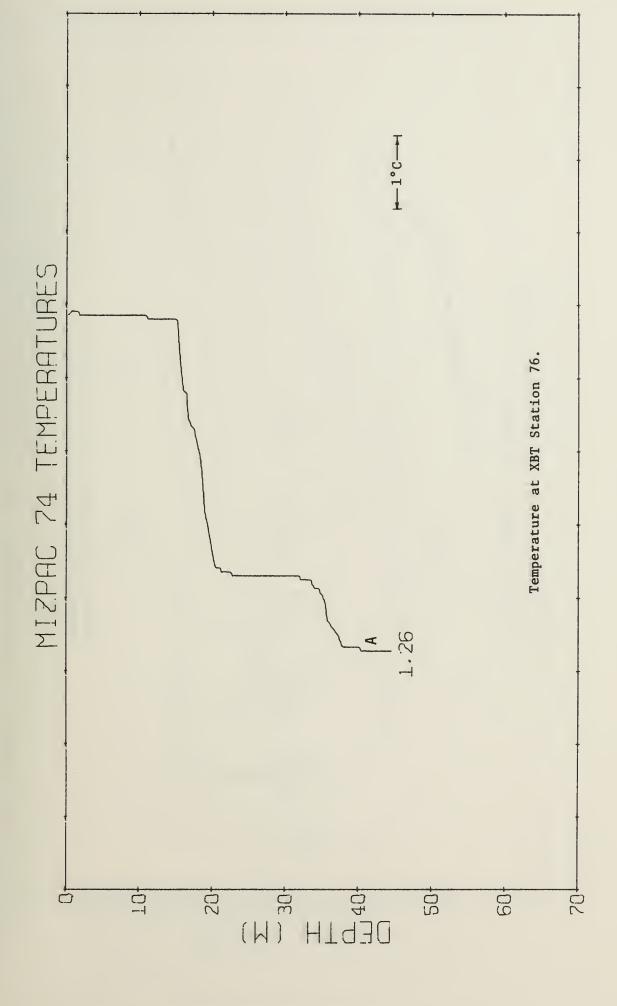


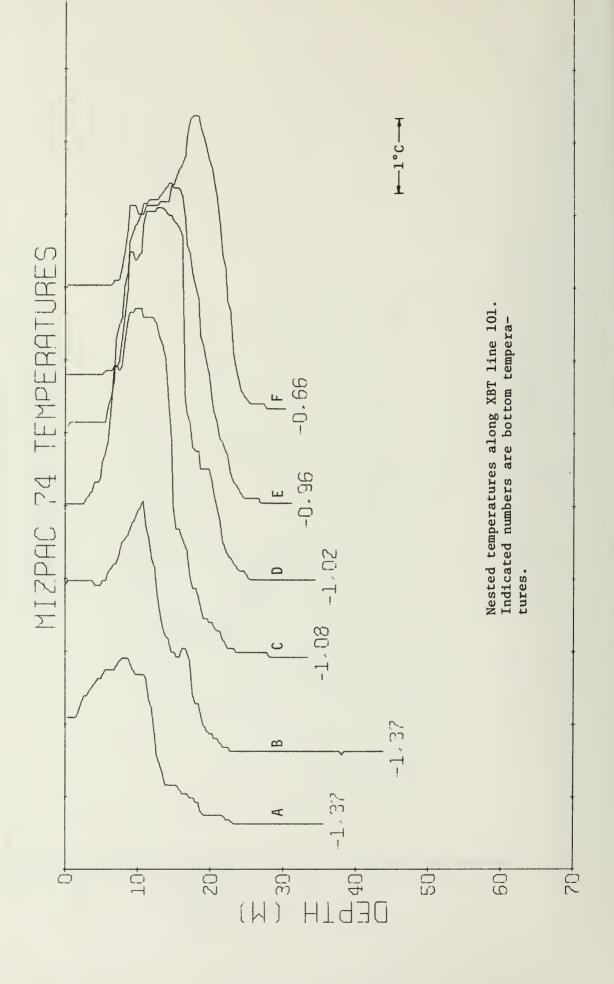


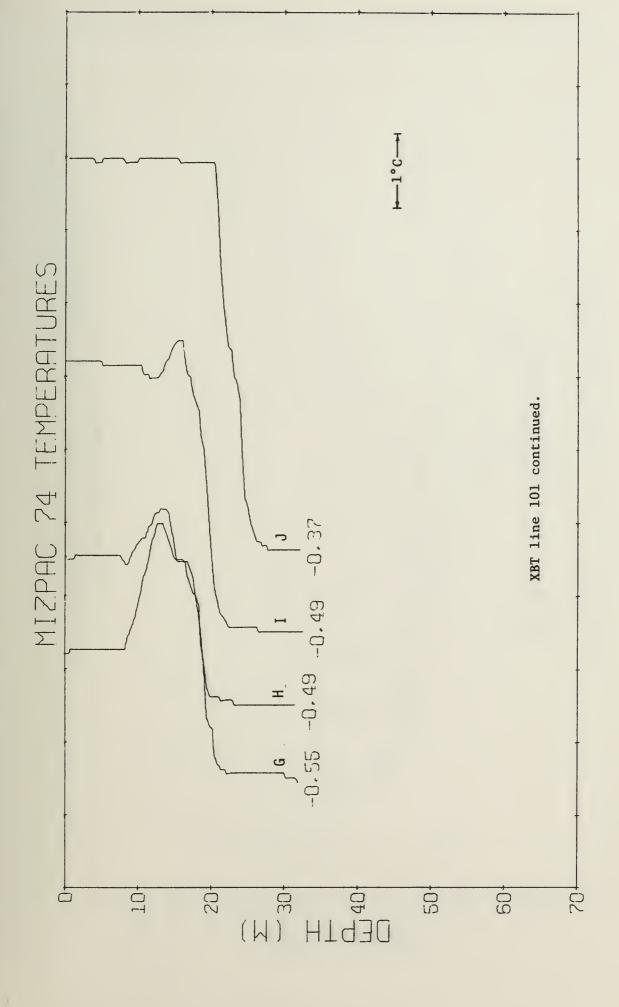


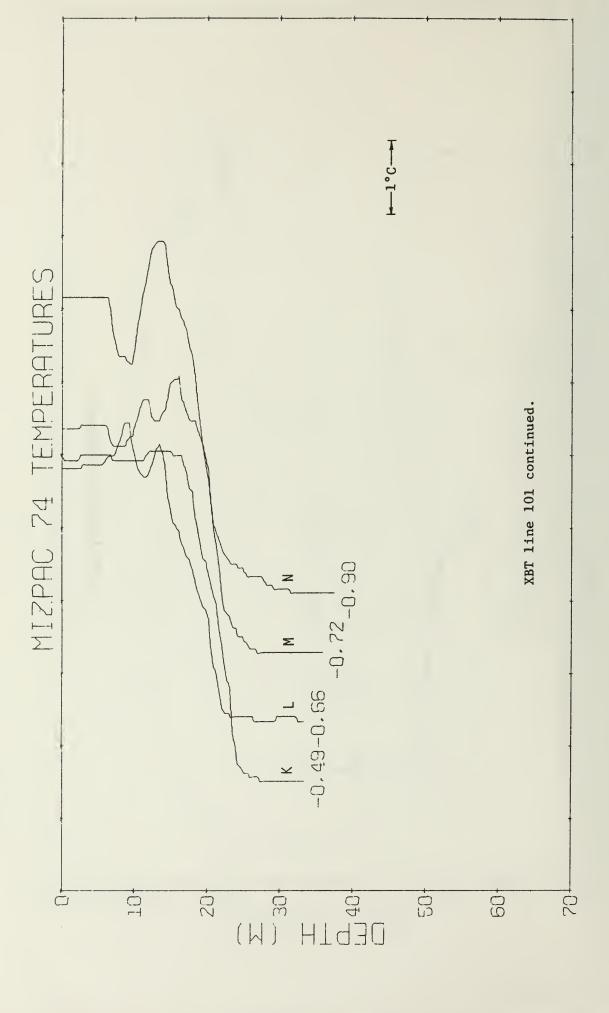


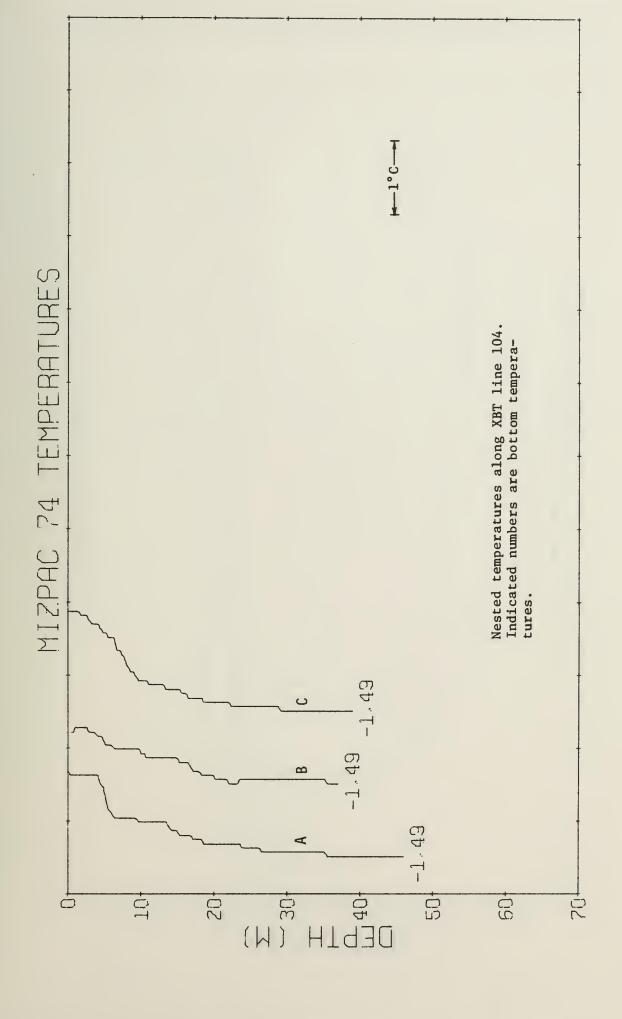


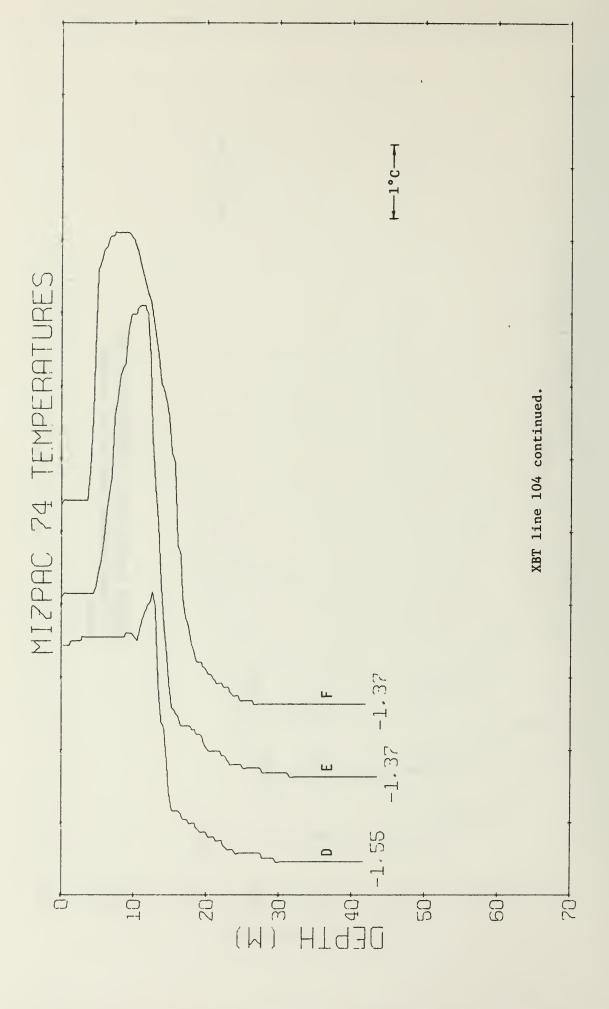


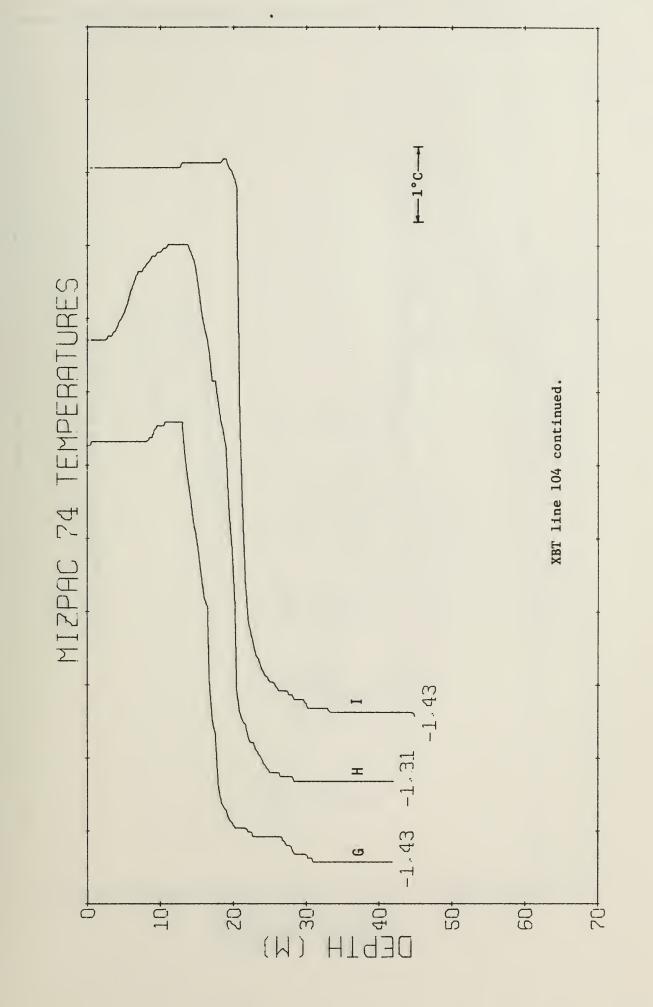


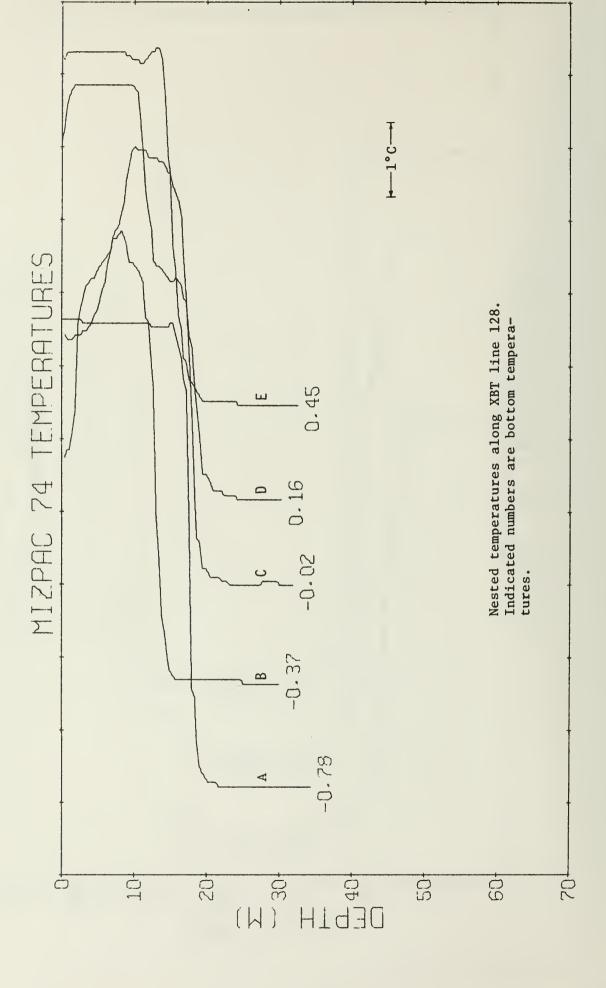


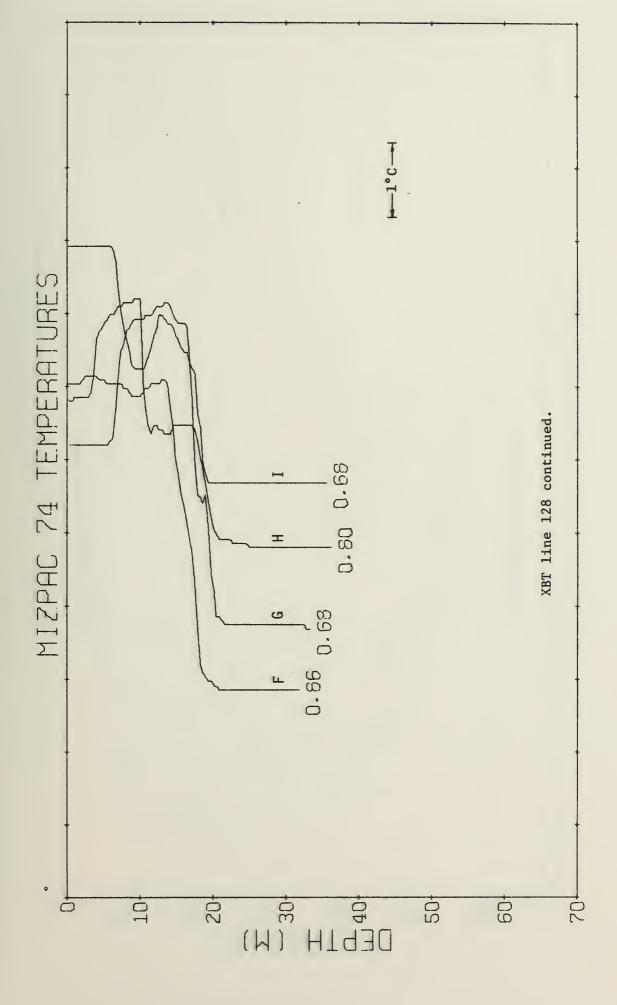


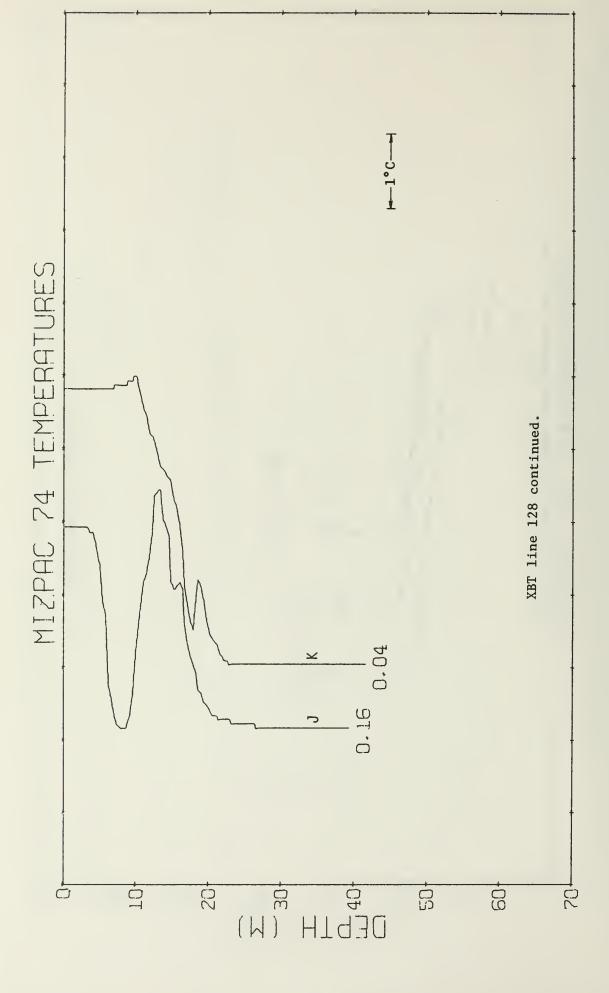


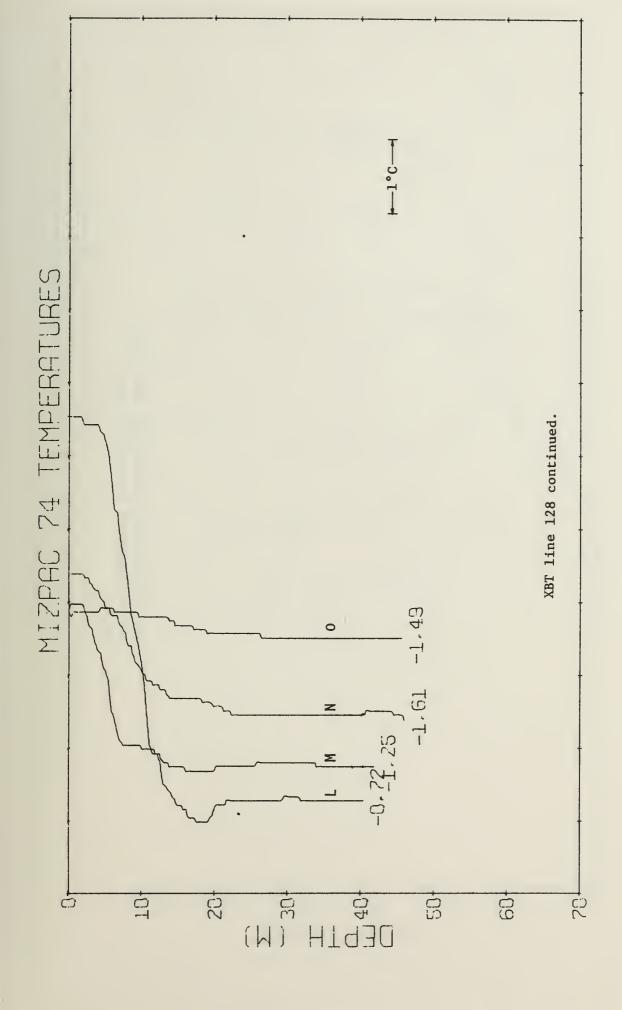


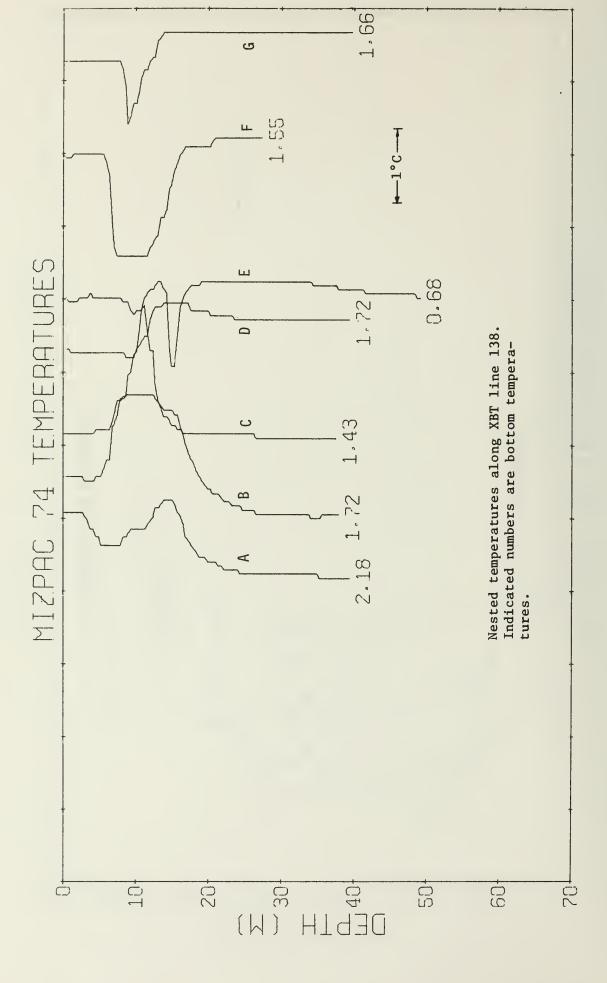


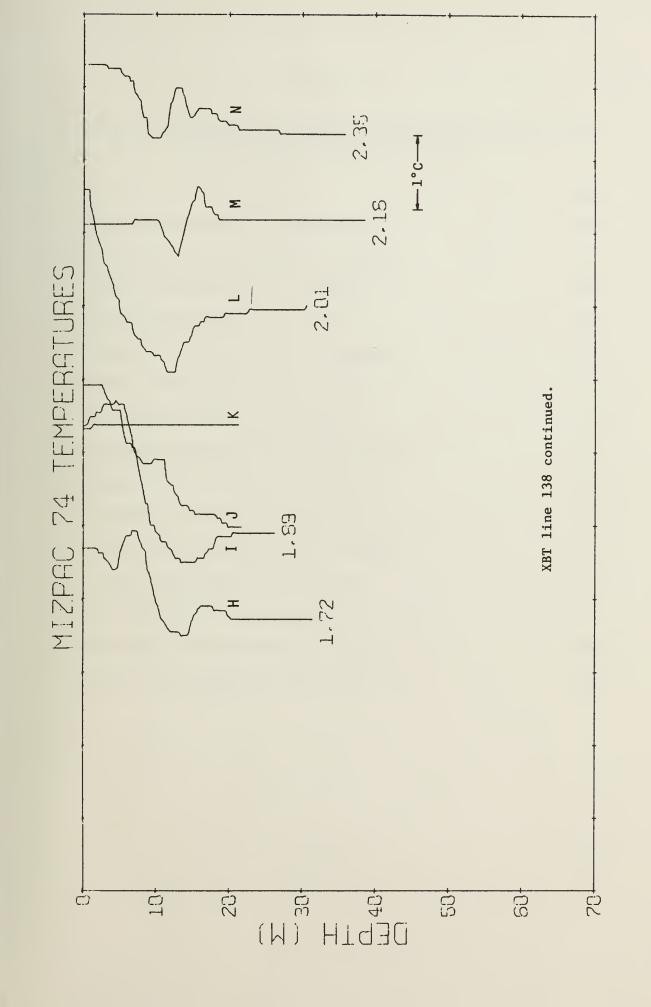


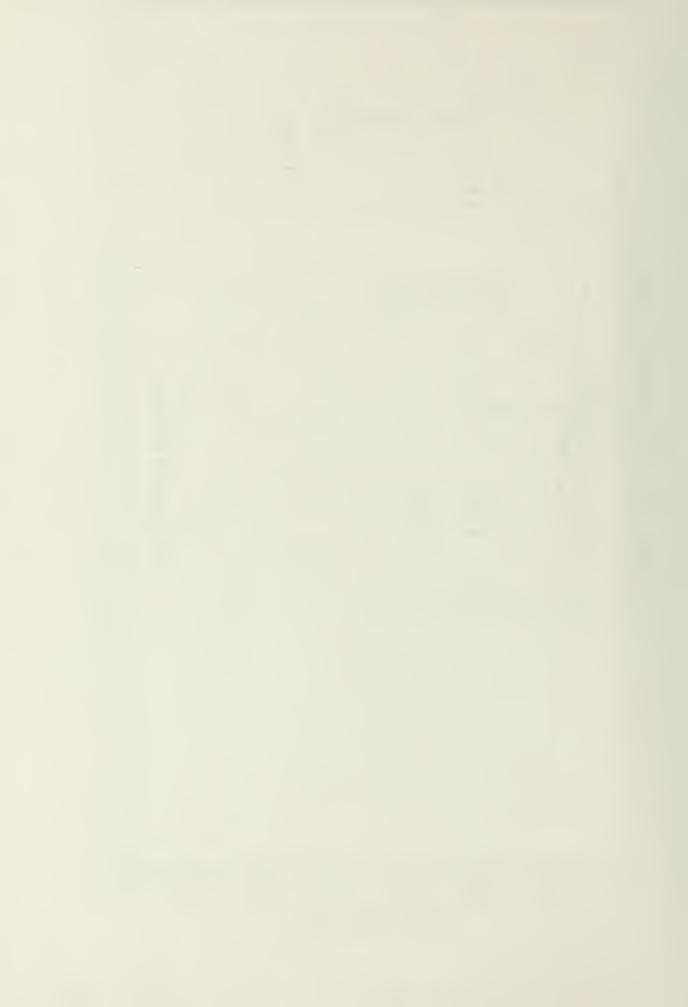








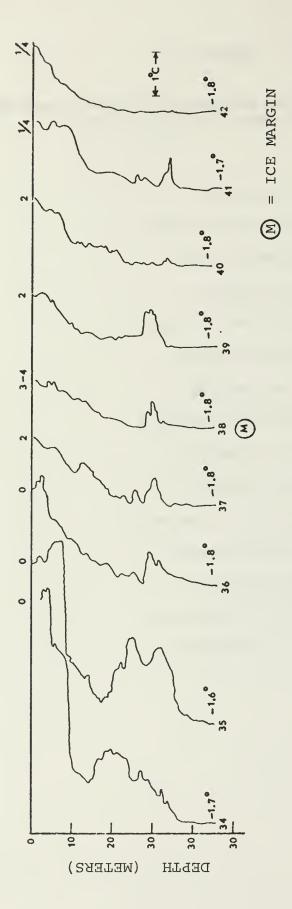




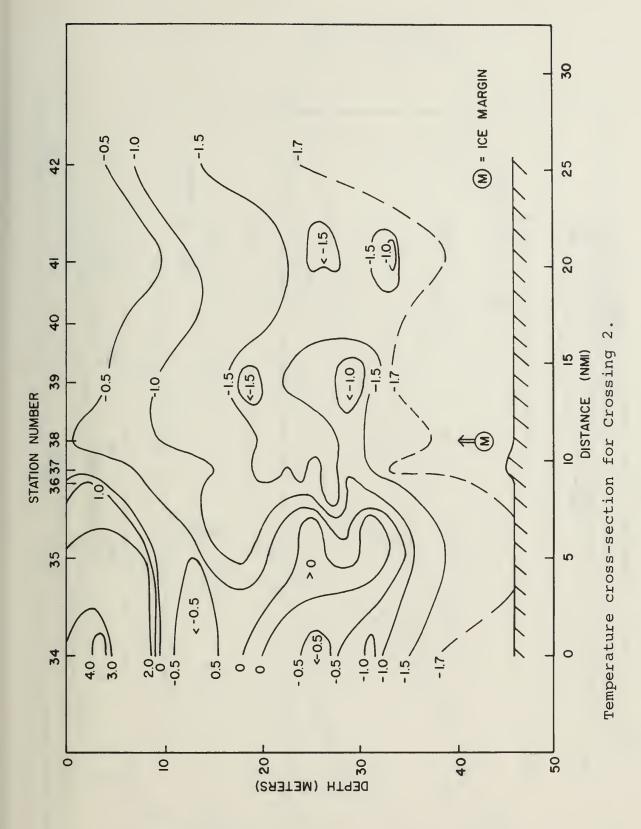
APPENDIX IV

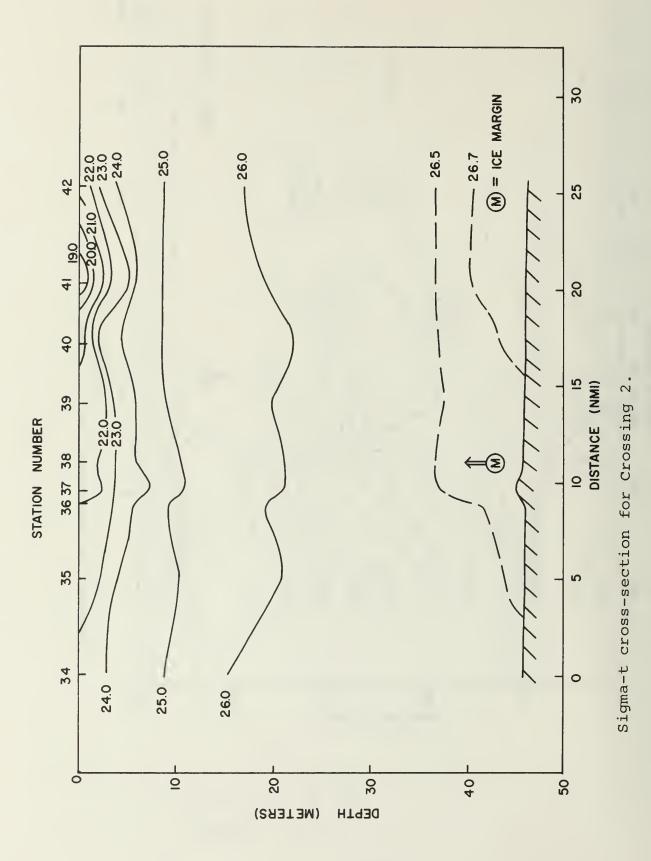
TEMPERATURE PROFILES AND TEMPERATURE AND SIGMA-T CROSS-SECTIONS FOR ICE MARGIN CROSSINGS 2-5 AND 7

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Temperature profiles for Crossing 2	IV-1
Temperature cross-section for Crossing 2	IV-2
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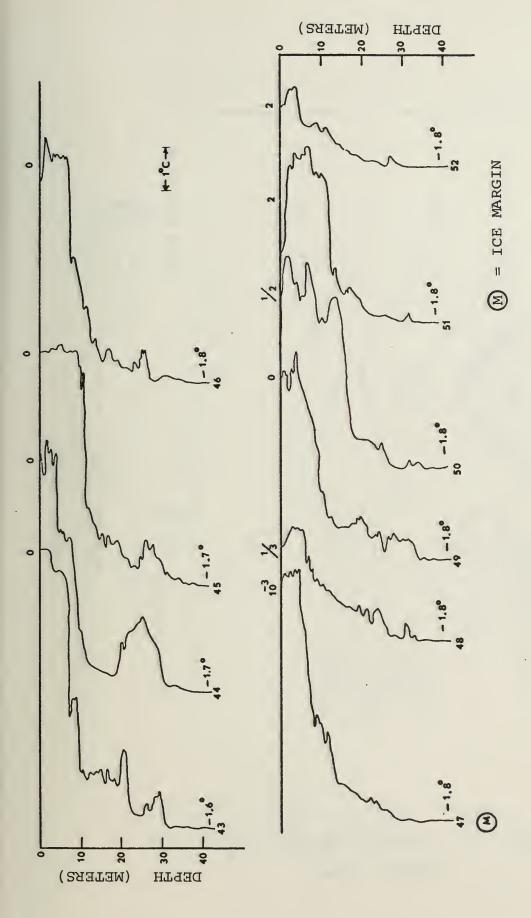


Numbers at the top of trace are ice concentrations; at the bottom of the trace the bottom temperature. Temperature profiles for Crossing 2.

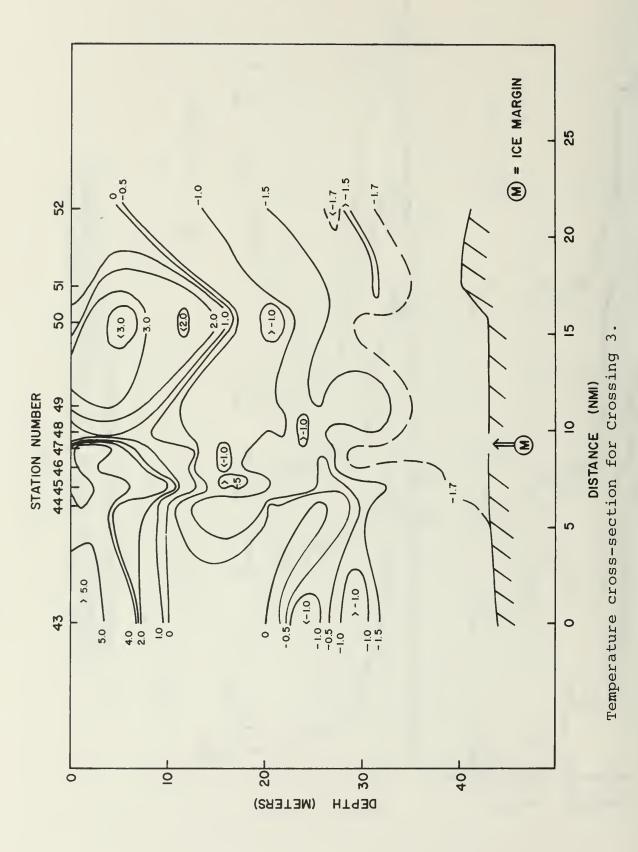


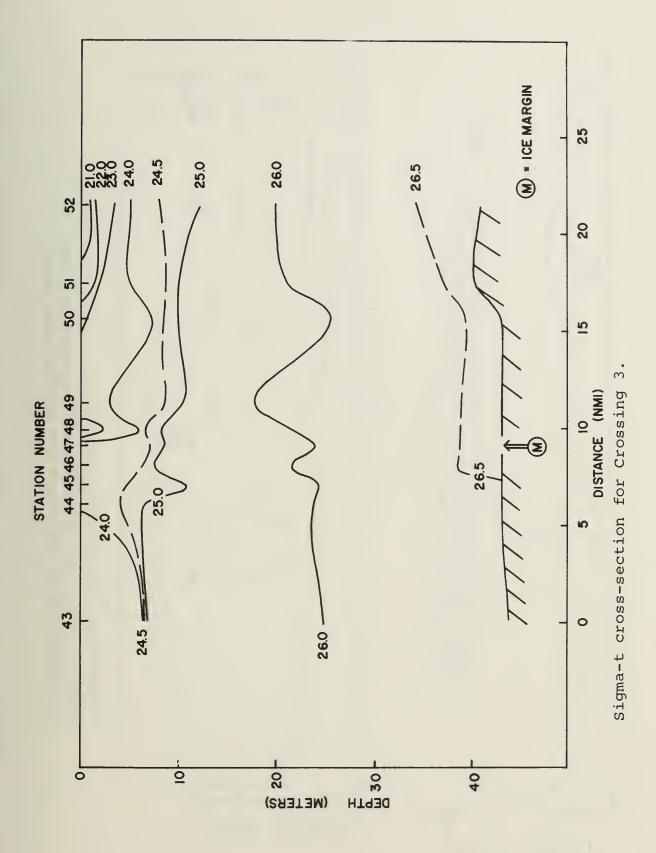


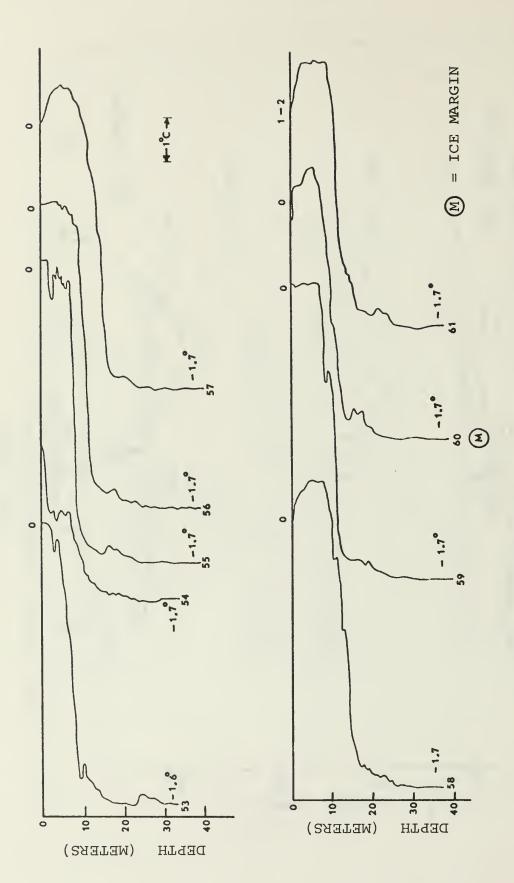
IV-3



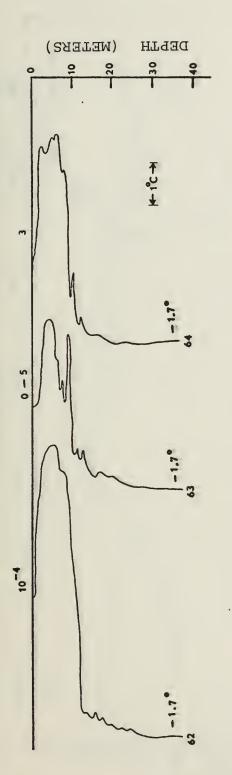
Temperature profiles for Crossing 3. Numbers at the top of trace are ice concentrations; at the bottom of the trace the bottom temperature.



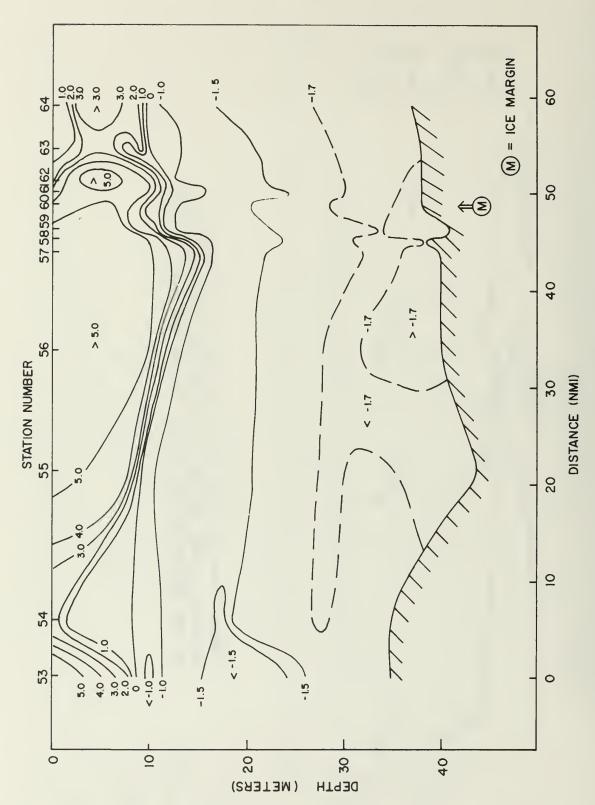




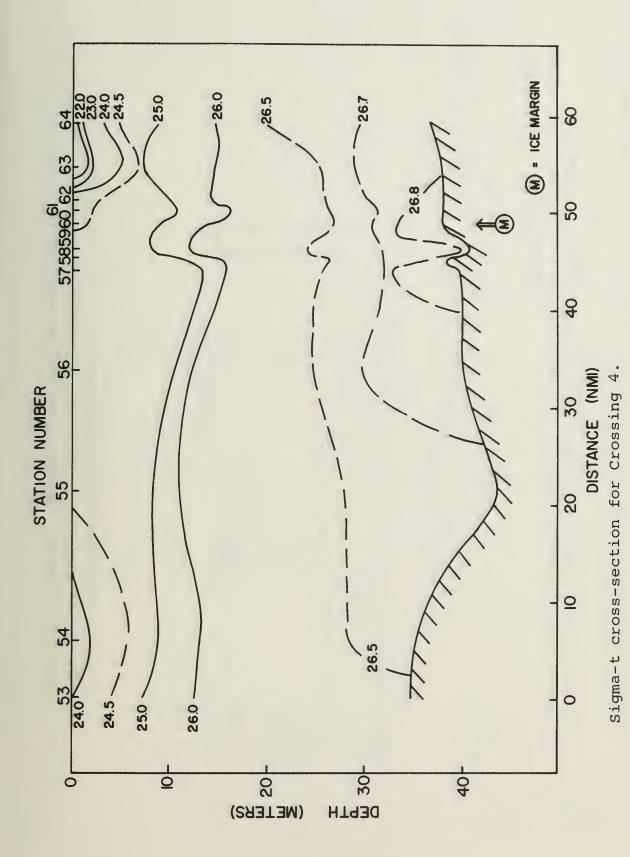
Numbers at the top of trace are ice concentrations; at the bottom of the trace the bottom temperature. Temperature profiles for Crossing 4.

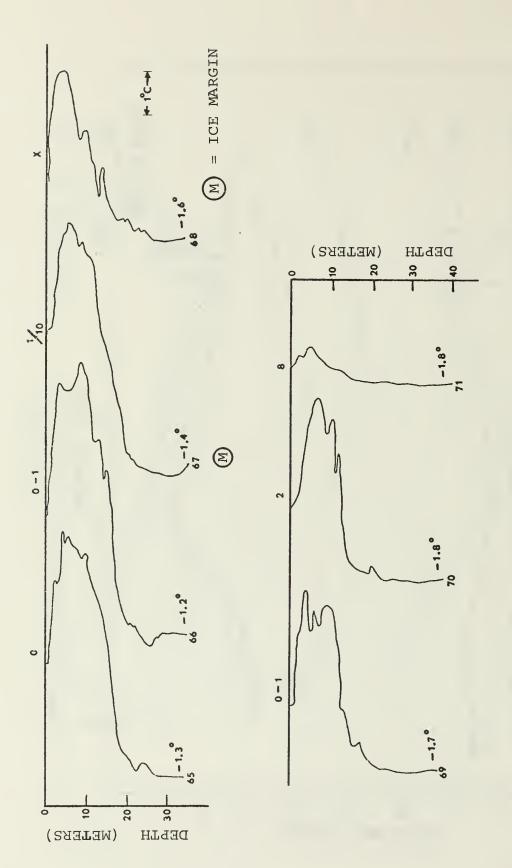


Numbers at the top of trace are ice concentrations; at the bottom of the trace the bottom temperature. Temperature profiles for Crossing 4, continued.

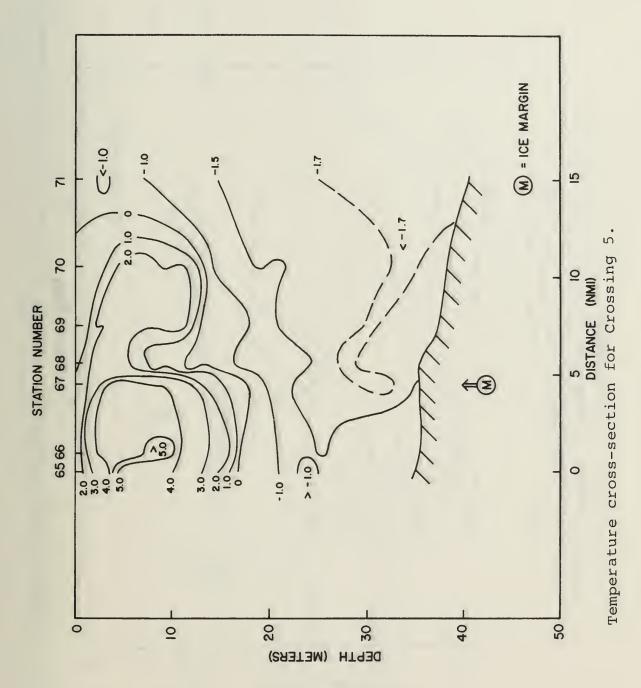


Temperature cross-section for Crossing 4.

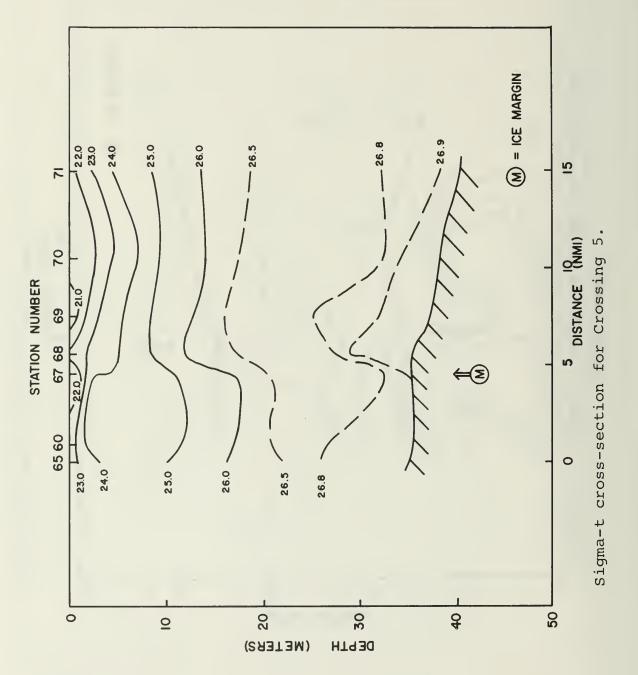


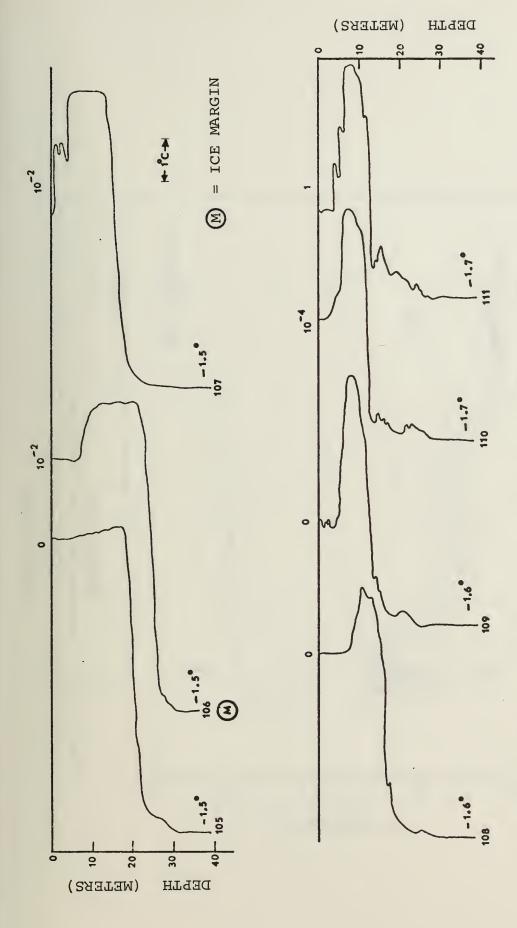


Numbers at the top of trace are ice concentrations; at the bottom of the trace the bottom temperature. Temperature profiles for Crossing 5.

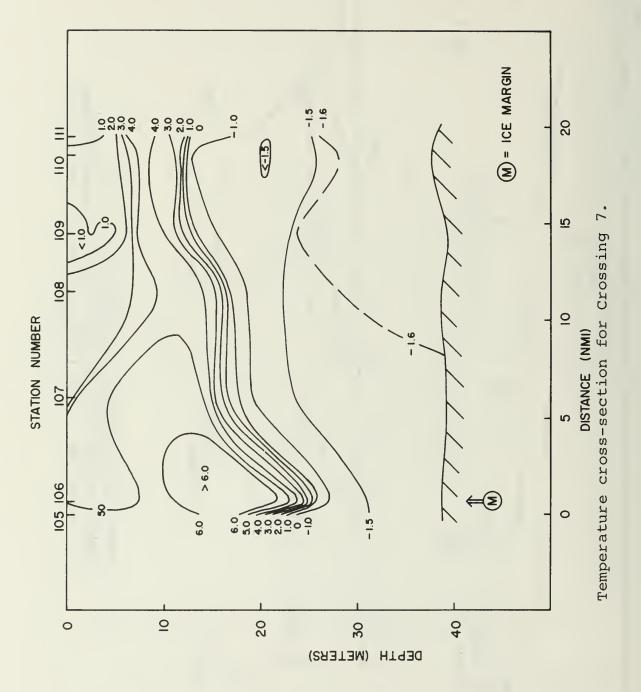


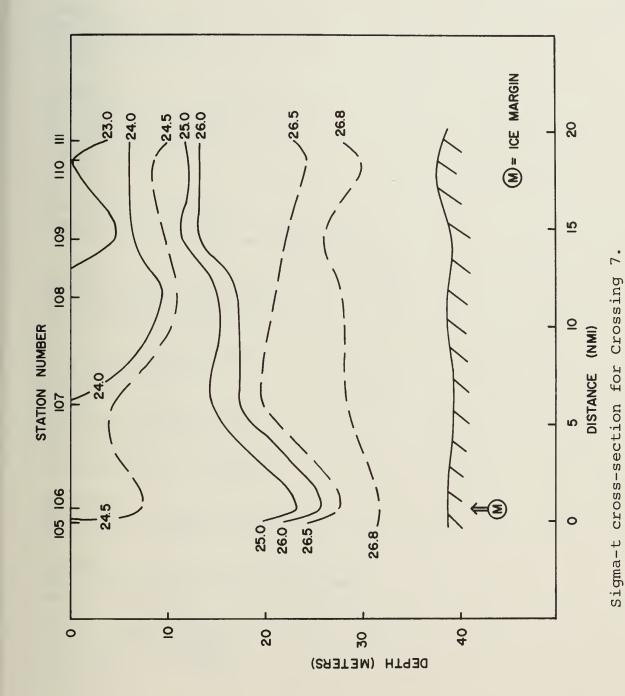
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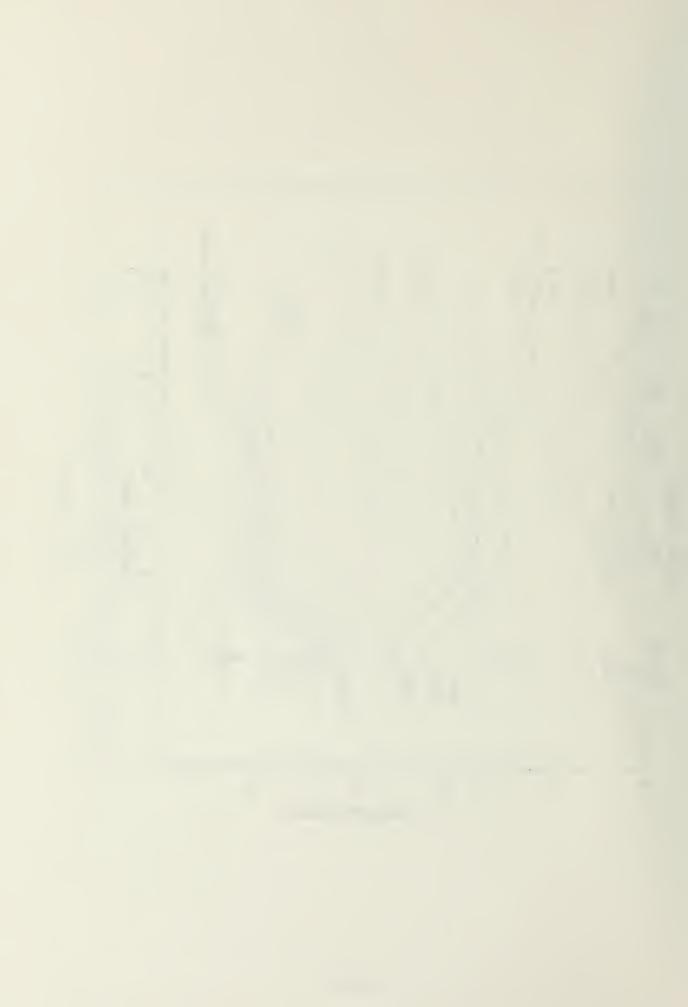


Numbers at the top of trace are ice concentrations; at the bottom of the trace the bottom temperature. Temperature profiles for Crossing 7.





IV-16



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